

Energy Harvester Powered Sensors: A Holistic Approach

Paul Mitcheson *et al*
EH Network 2013 meeting

Outline

Overview of a recently completed EPSRC project:

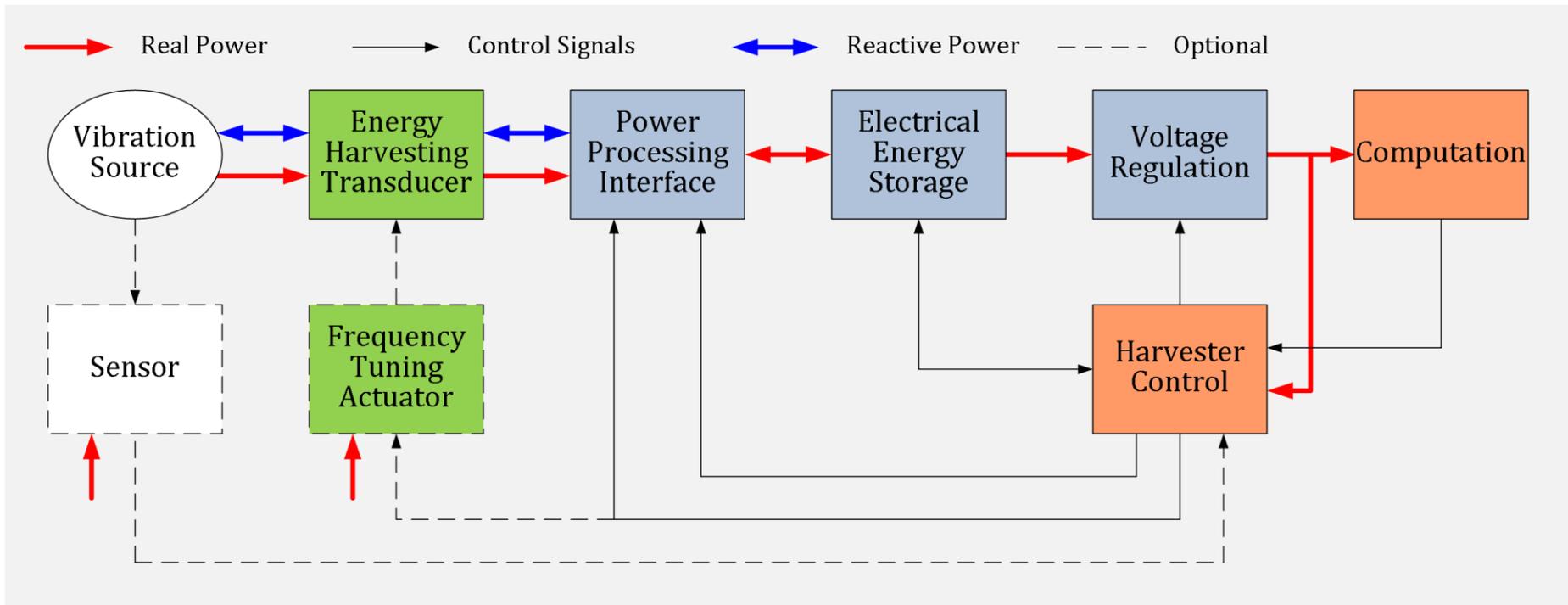
Next Generation Energy-Harvesting Electronics: A Holistic Approach

Four main areas, highlights of each:

- Adaptive Harvesters
 - Power Electronics
 - Energy Modulated Computation
 - Modelling
- } *Closely related*



The System



Theme A has run throughout the project and involves Imperial, Bristol and Southampton

Adaptive Harvesters and Power Electronics

Adaptive Harvester

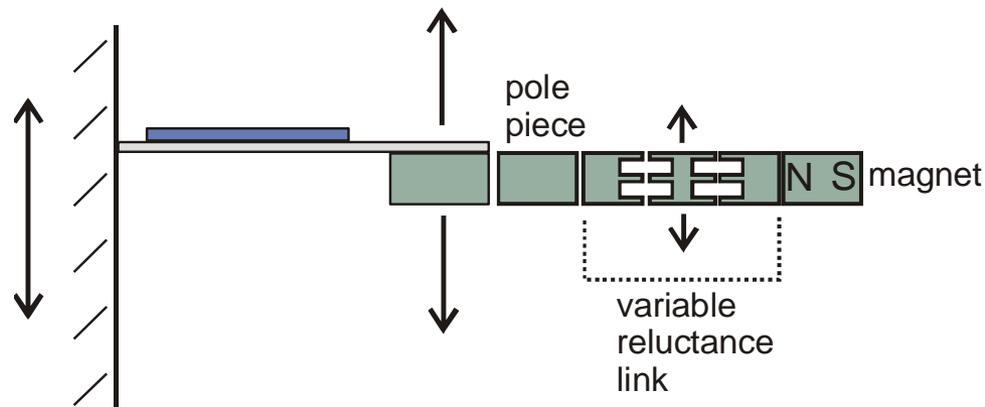
Two degrees of freedom in a motion driven harvester:

- Tuning Frequency
 - Investigated here with variable reluctance to create a magnetic potential well (in contrast to broadband techniques)
- Tuning Electrical Damping
 - Investigated using MPPT control of a boost rectifier and with piezoelectric harvesters and single-supply pre-biasing

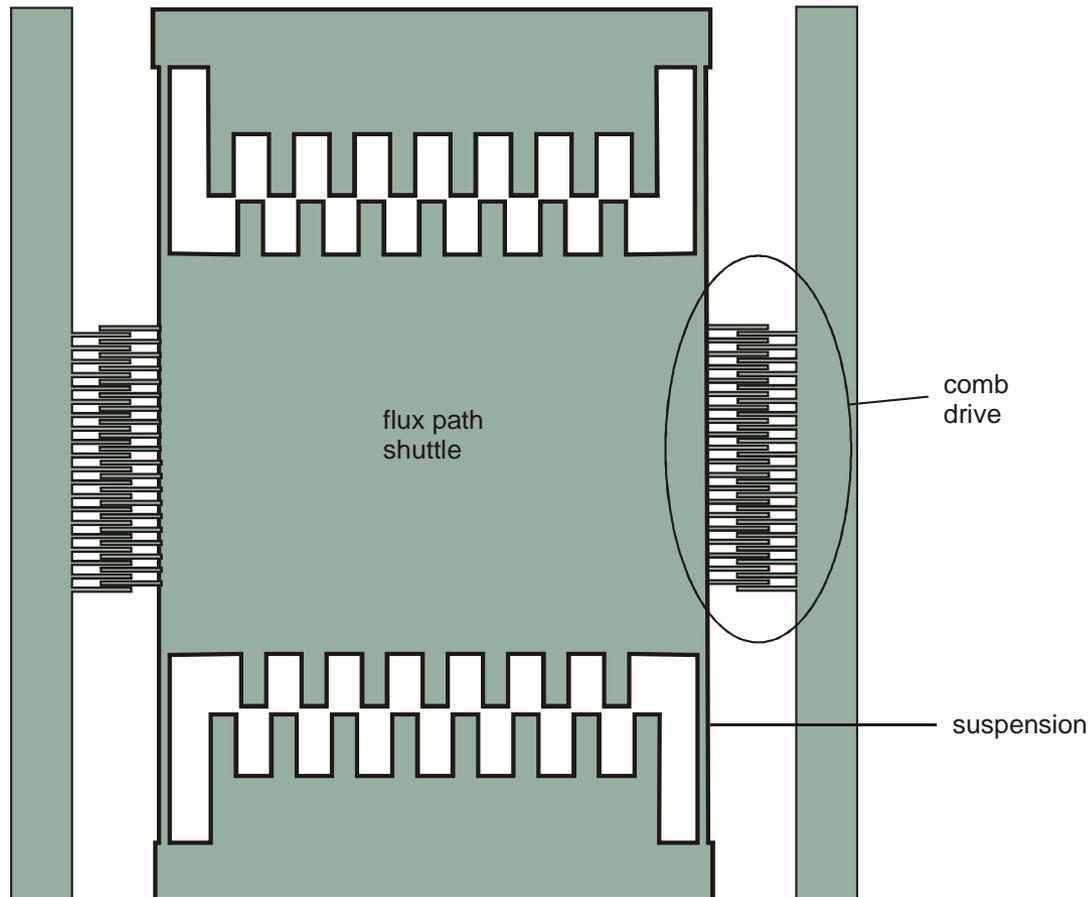
Tuning both of these is important in many real world applications – where excitation frequency and amplitude change

Basic Concept – Magnetic Potential Well

- Variable reluctance link
- Use permanent magnet, linked to oscillating proof mass by low reluctance path to pole piece
- Vary reluctance of this path by introducing a variable air gap
- Control this gap by MEMS electrostatic actuator
- This arrangement means the MEMS structure doesn't need a permanent magnet on the moving part – making fabrication and assembly easier



MEMS VRD

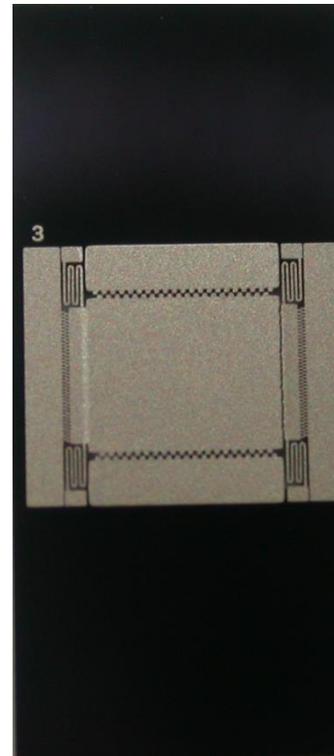


- Electrostatically actuated
- Alter magnetic reluctance between each end of the VRD

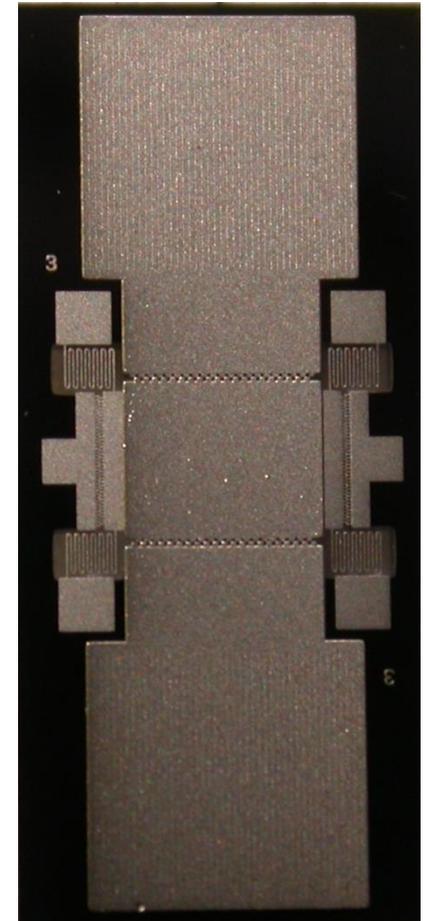
Picture of Fabricated MEMS VRD



Die size comparison

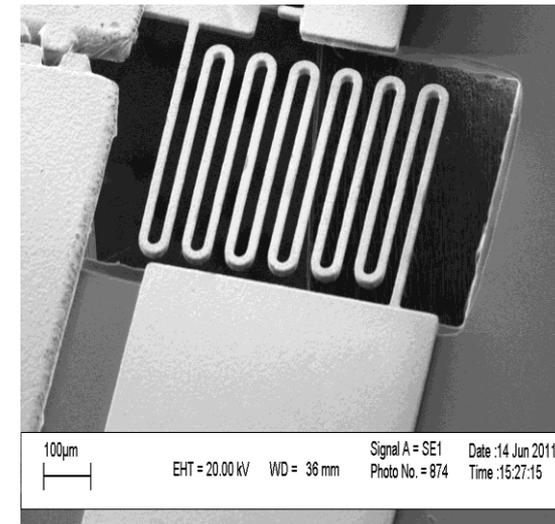
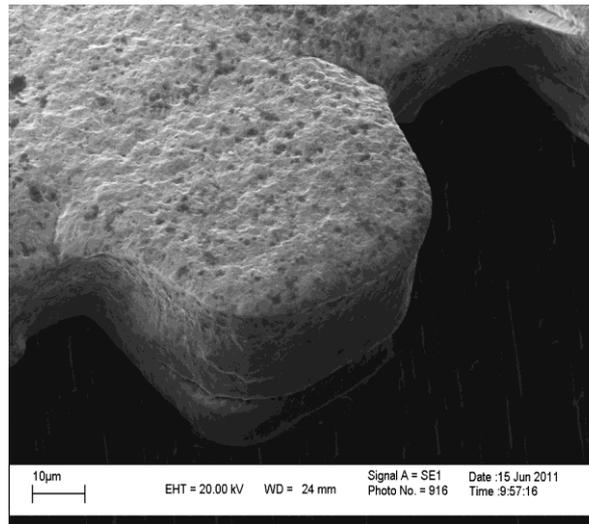
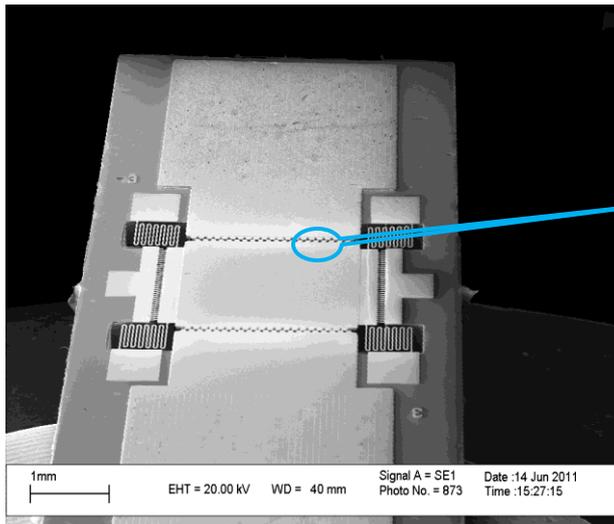
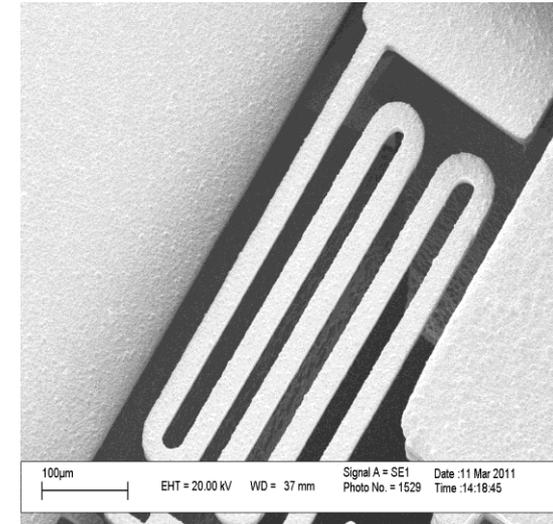
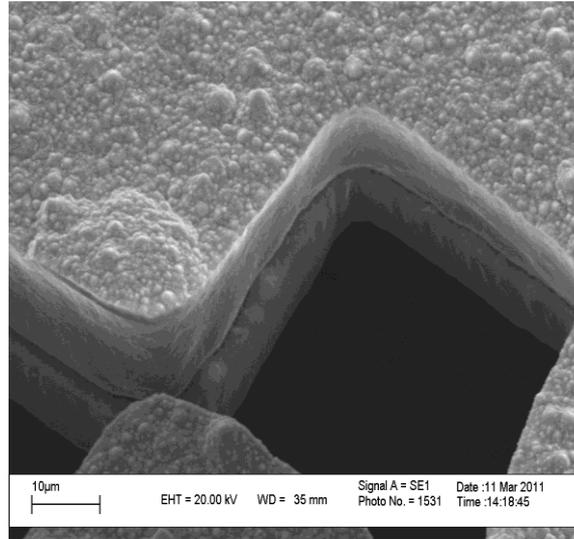
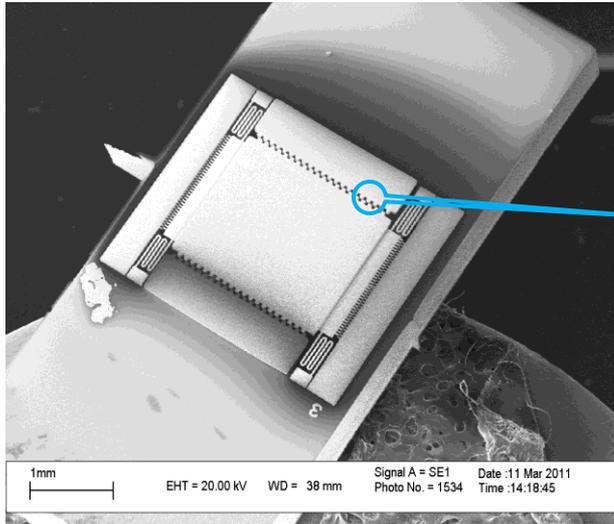


Previous fabricated die

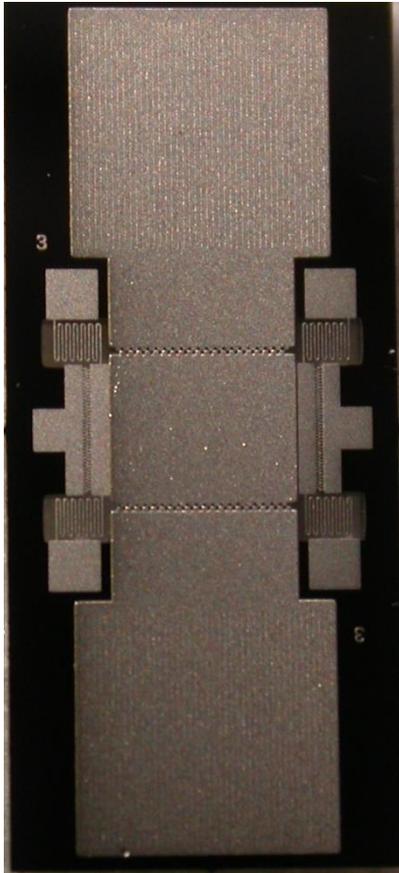


Recent Fabricated Die

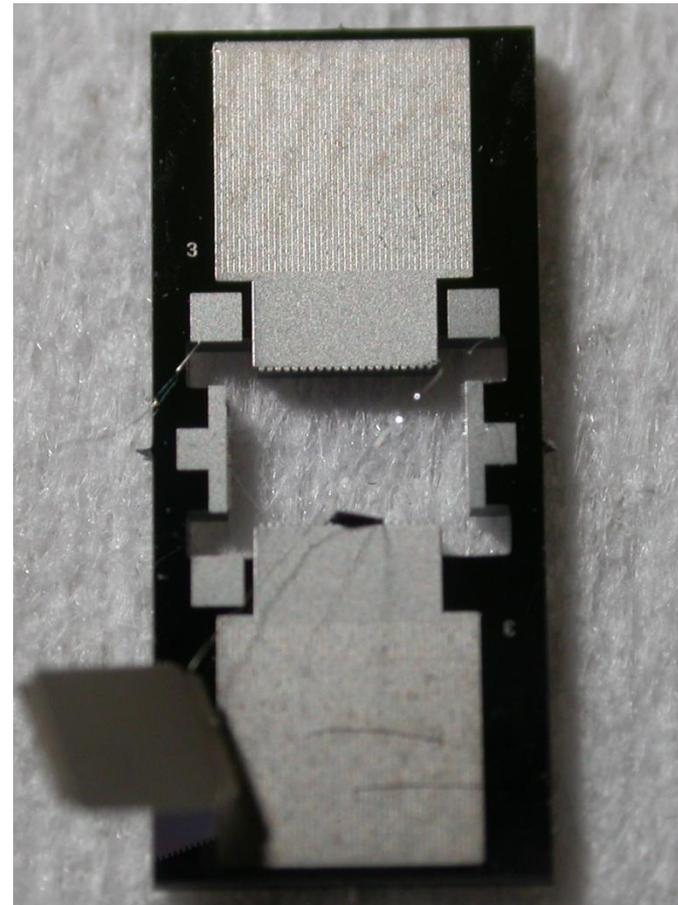
SEM Picture of the fabricated device



VRD Difficulties - Manual Placement of Magnet



*Before placing magnet on
VRD*



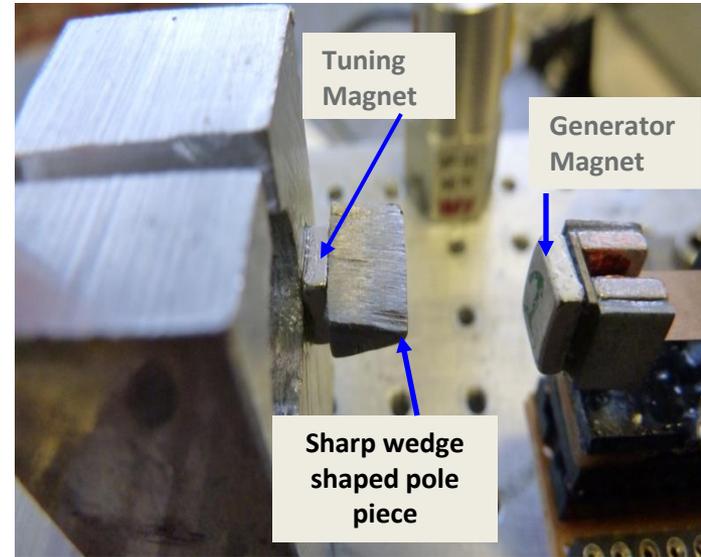
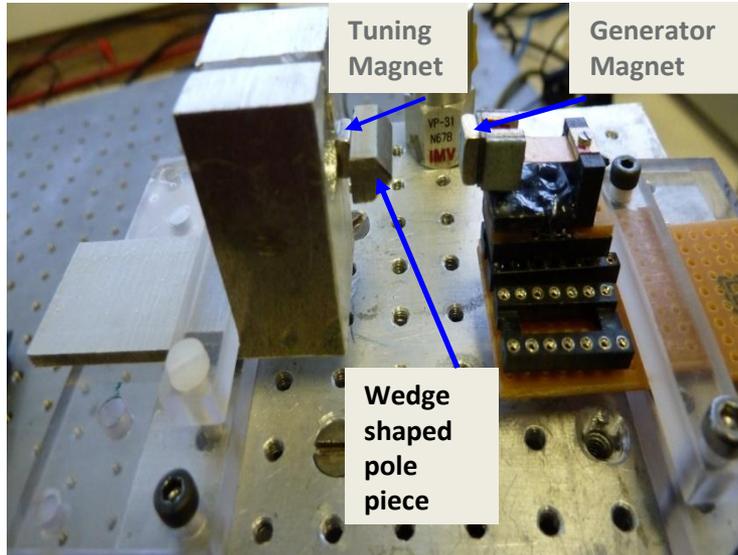
*Movable part of VRD has pulled off
due to magnetic force and broken
the die*

Macroscale Prototype

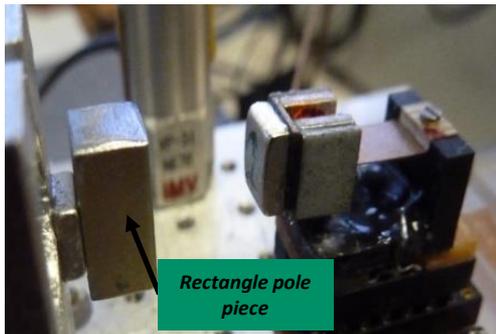
- The MEMS VRD was unable to generate sufficient changes in force to show a good tuning range.
- In order to demonstrate the effect of a magnetic potential well on tuning, a macro scale prototype was created
- Significantly less force can be achieved to perform tuning by creating a magnetic potential well, rather than simply straining a cantilever
- Various experiments were conducted to measure the force required to tune, using shaped pole pieces

Magnetic tuning: Effect of field shape

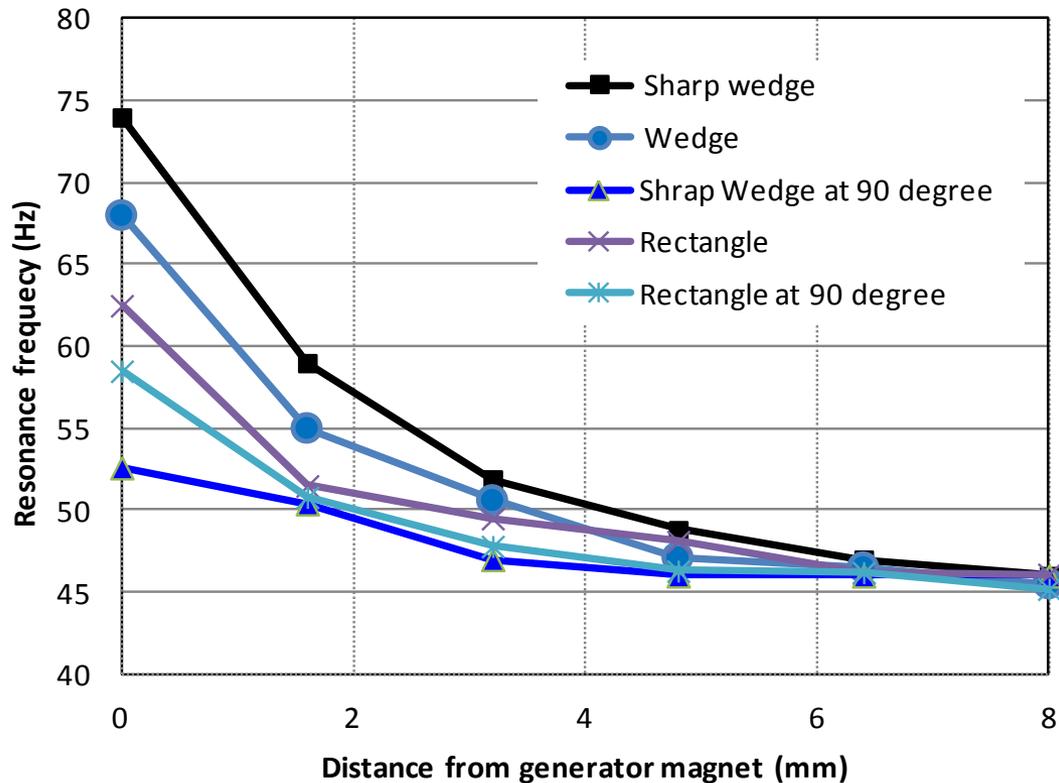
Test arrangement with sharp wedge shape pole piece



Test arrangement with wedge shape pole piece

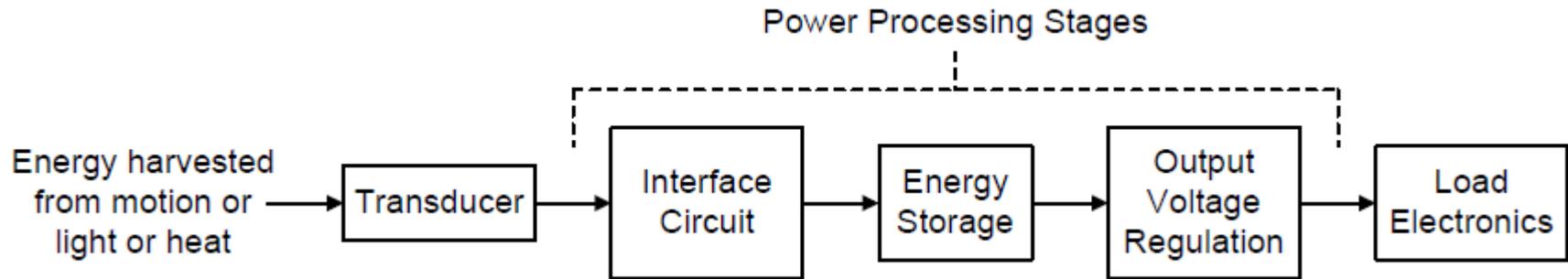


Shaped Pole Piece Tuning Results



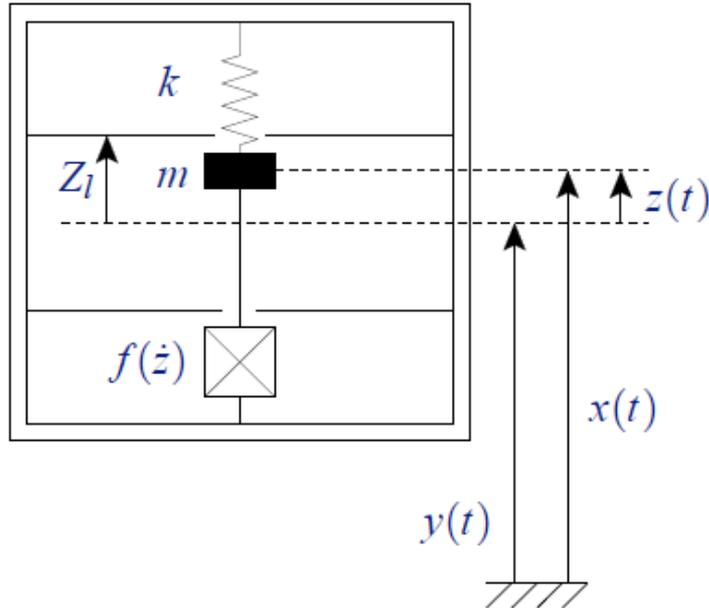
- Significant improvement in tuning of +/- 20% using sharp wedge
- Shape has major impact in tuning range

Power Electronics – Optimised Damping



- The energy harvesting system must have a power processor stage between the transducer and storage element – at least for rectification
- In Holistic, we have looked at circuits for both electromagnetic harvesters and piezoelectric harvesters

Inertial Generators



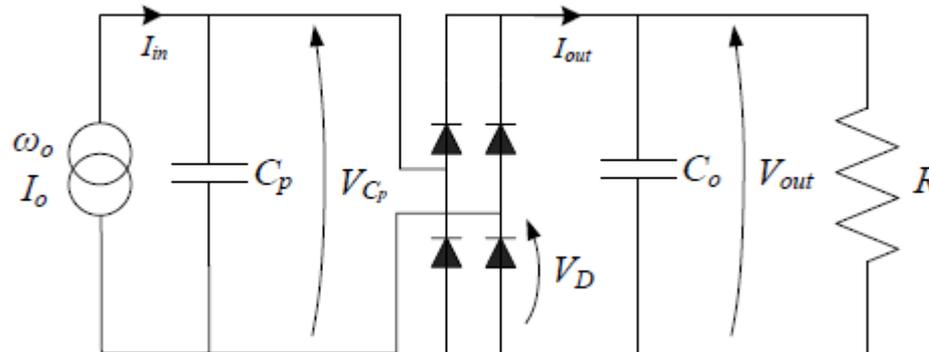
- We need to set the value of the damper to maximise the generated power.
- The optimal electrical damping maximises the force-distance integral of the damper
- Too low, no force
- Too high, no displacement

We have investigated circuits to optimise the damping

Piezoelectric Harvesters

Piezoelectric harvesters produce AC outputs

- Must have rectification
- May require step up or down depending on open circuit voltage of piezo.
- Simplest circuit we can think of is a full bridge rectifier:

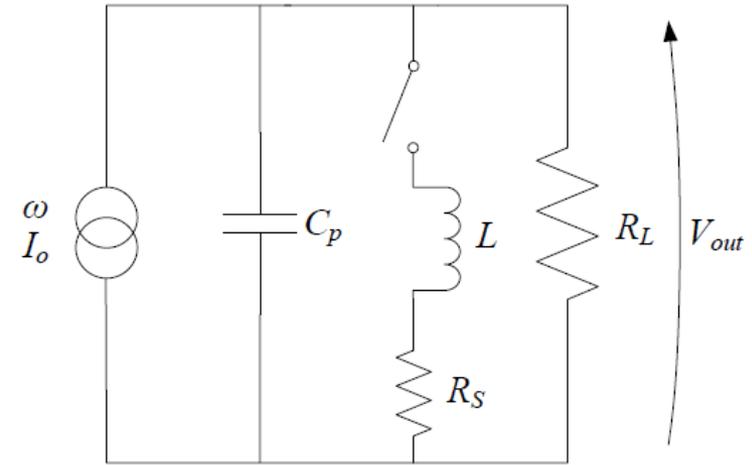
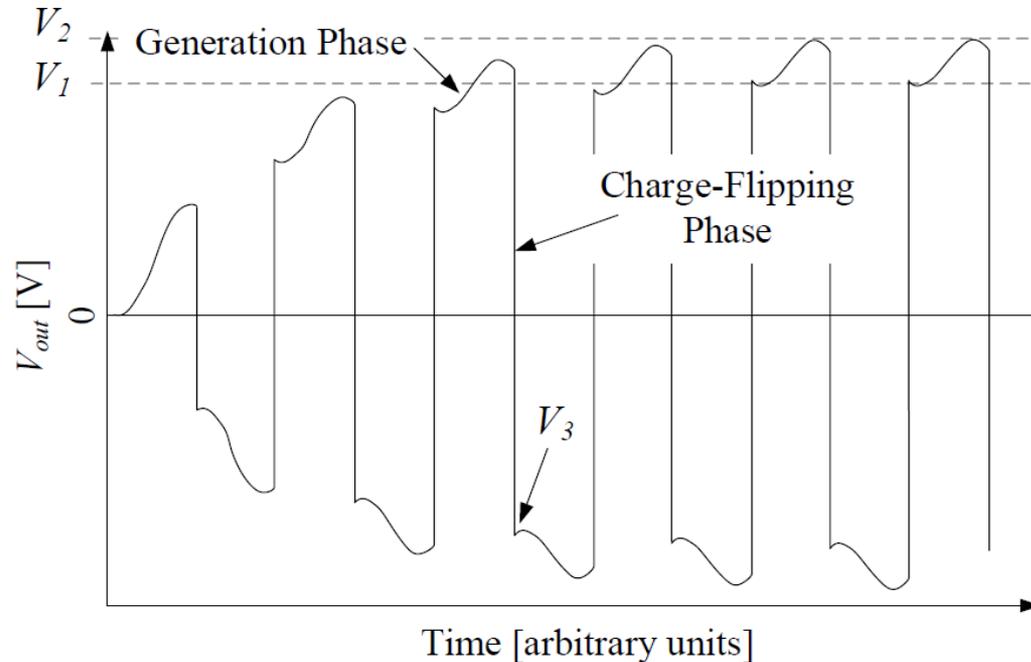


Target is to achieve the optimal damping and rectify the signal simultaneously

- Can we achieve optimal damping (maximum power) with this interface?

Synchronous Switched Harvesting

Guyomar et al.

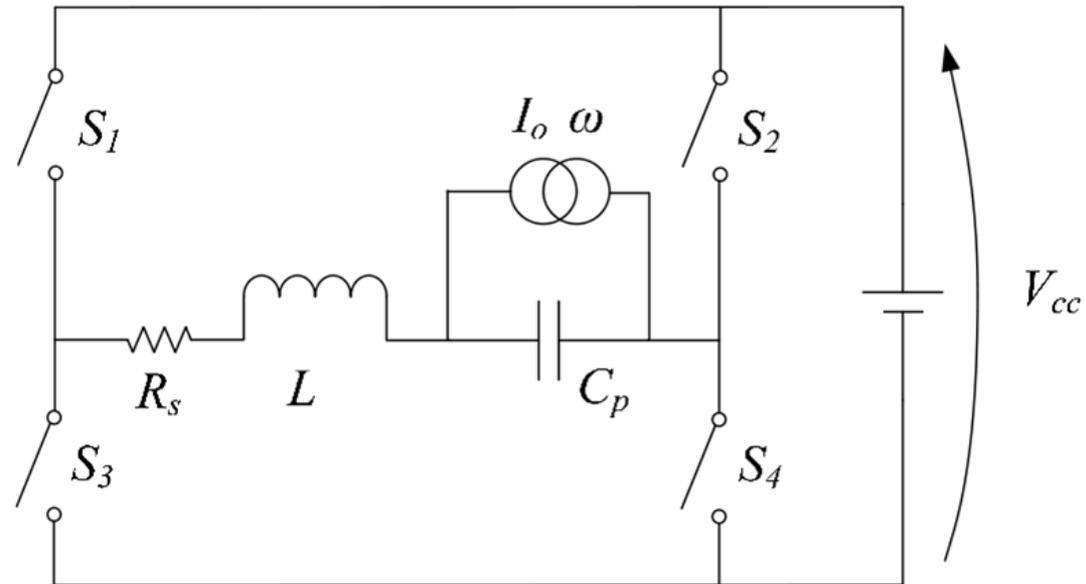


Often referred to as SSHI

- Charge on capacitor is resonantly flipped at voltage peaks to build piezo voltage
- Increases damping force and power

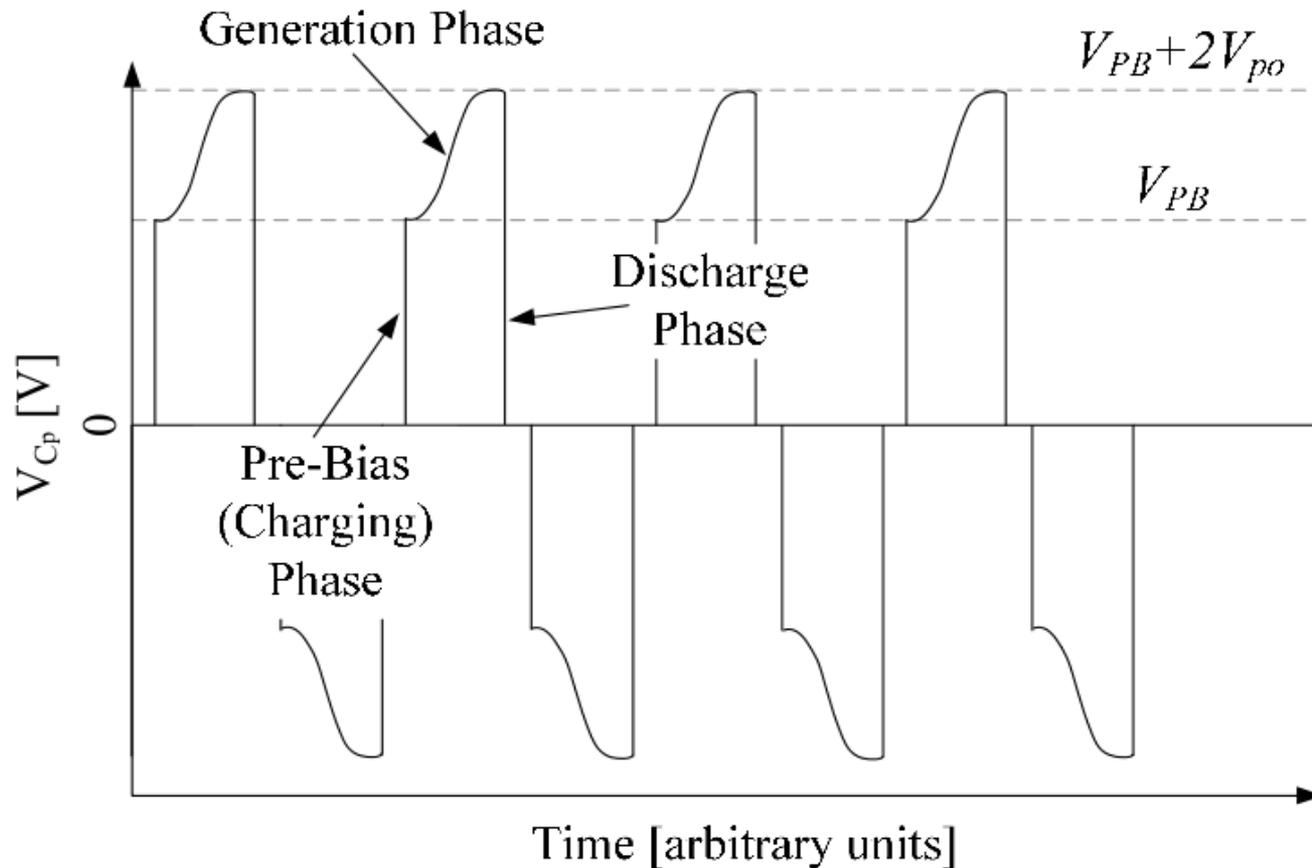
Single Supply Pre-biasing Circuit Overview

- Single source pre-bias circuit
- Source supplies pre-charge
- Generated energy returned to same source
- Can be made diode-less (with no free wheeling currents) if V_{CC} is optimally set



Let's see how it works...

Single Supply Pre-biasing Waveform



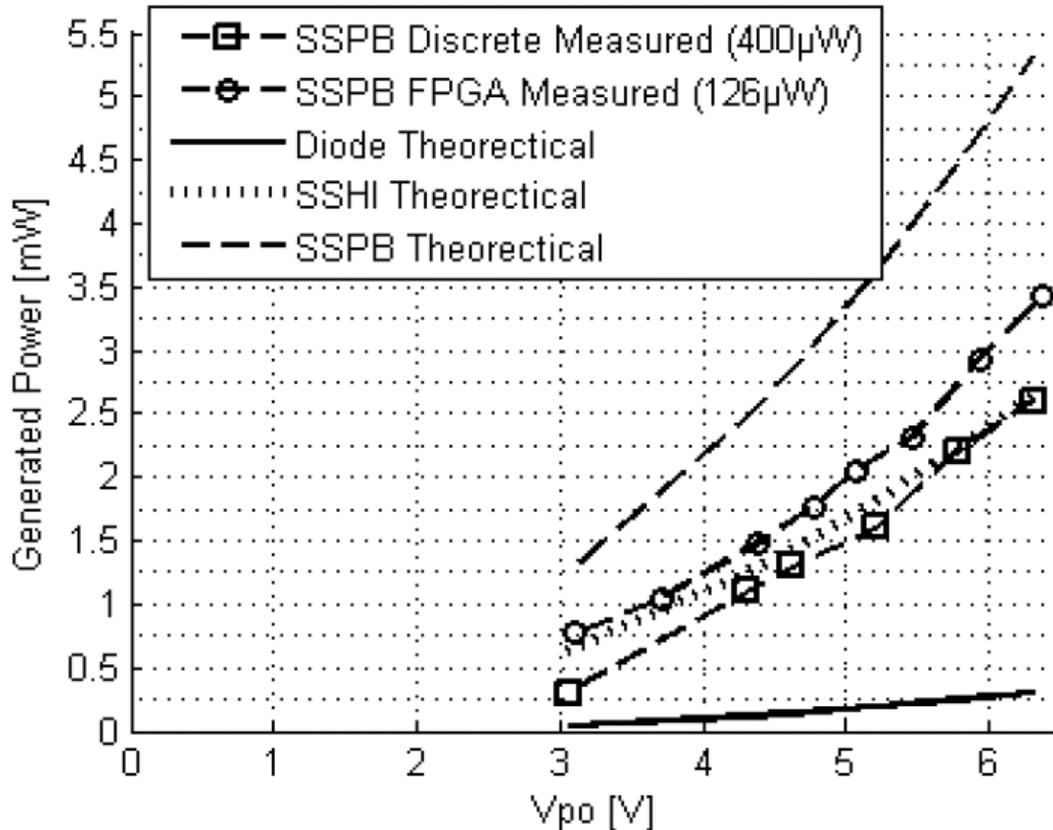
Operation similar to other synchronous circuits but charge "flipping" is in two stages

Power Output Formula

$$P_{\max} = V_{po}^2 f_o C_p \left(\frac{8Q}{\pi} \right)$$

- V_{po} is the open circuit voltage of the piezo
- f_o is the mechanical excitation frequency
- Q is the quality factor of the resonant charging path
- C_p is the capacitance of the piezo

Power Comparison

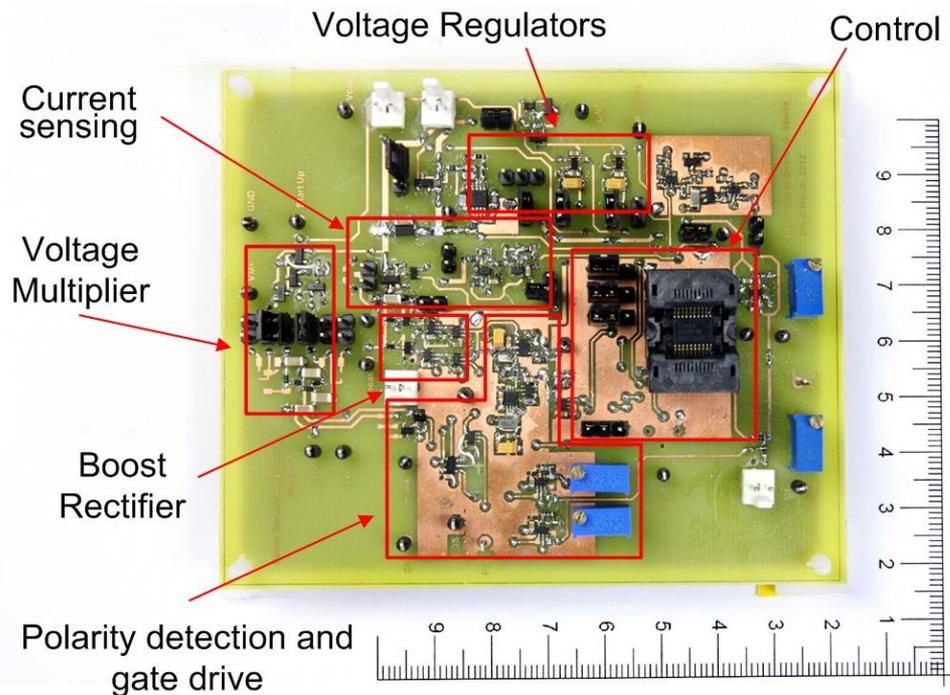


- Vast improvement over bridge rectifier
- SSPB practical implementation is better than the best possible performance of SSHI (even allowing for zero control overhead on SSHI)

For a review on all types of piezo interface circuits:

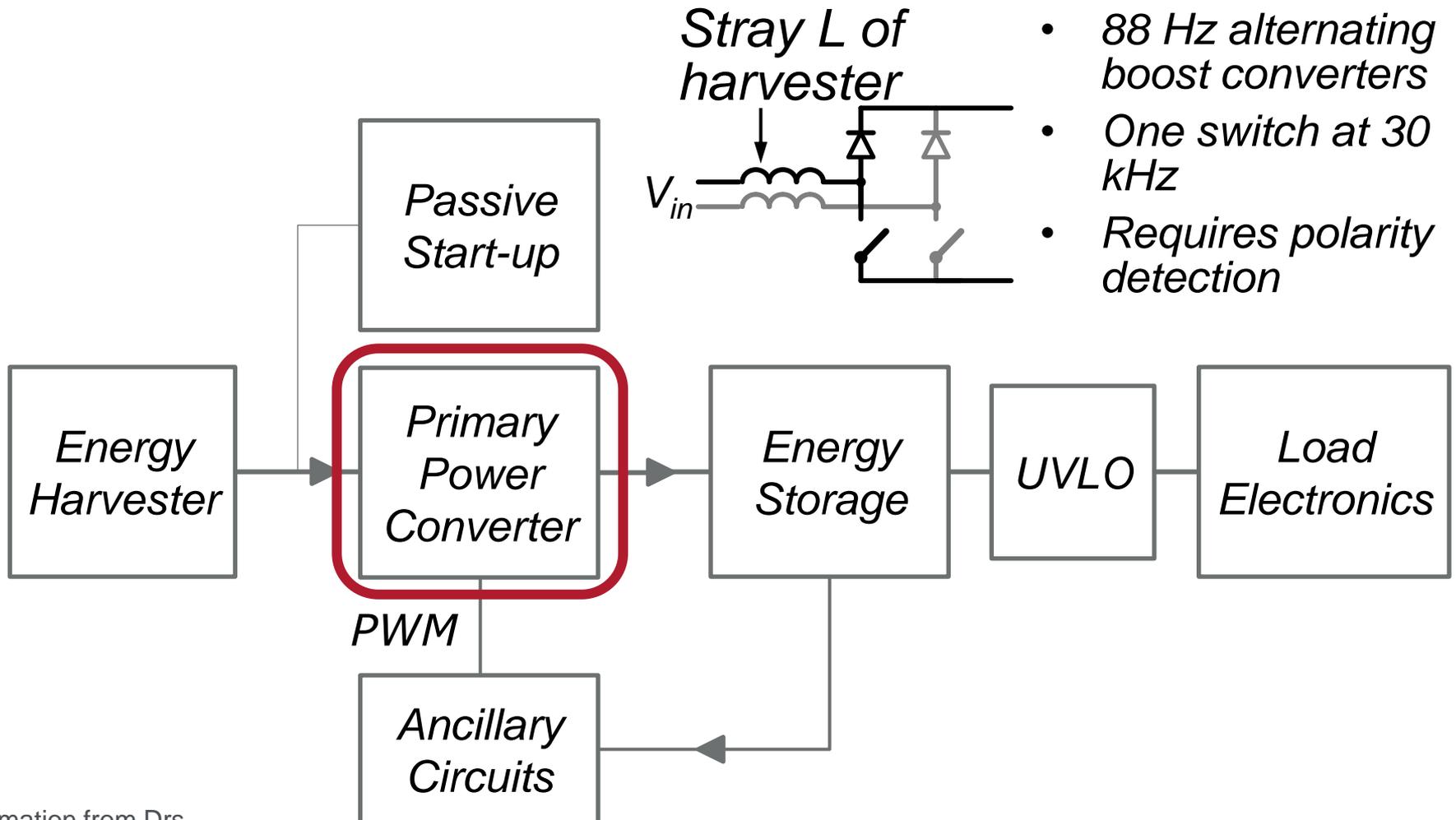
Dicken J, Mitcheson PD, Stoianov I, Yeatman, EM, **Power-Extraction Circuits for Piezoelectric Energy Harvesters in Miniature and Low-Power Applications**, IEEE Transactions on Power Electronics, 2012, Vol:27, Pages:4514-4529, ISSN:0885-8993

Interface Circuits for Electromagnetic Harvester



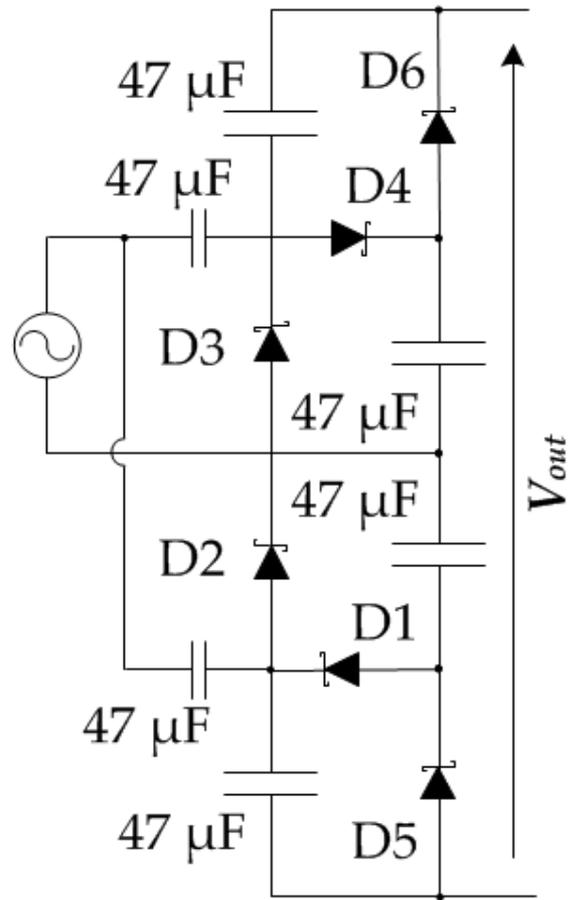
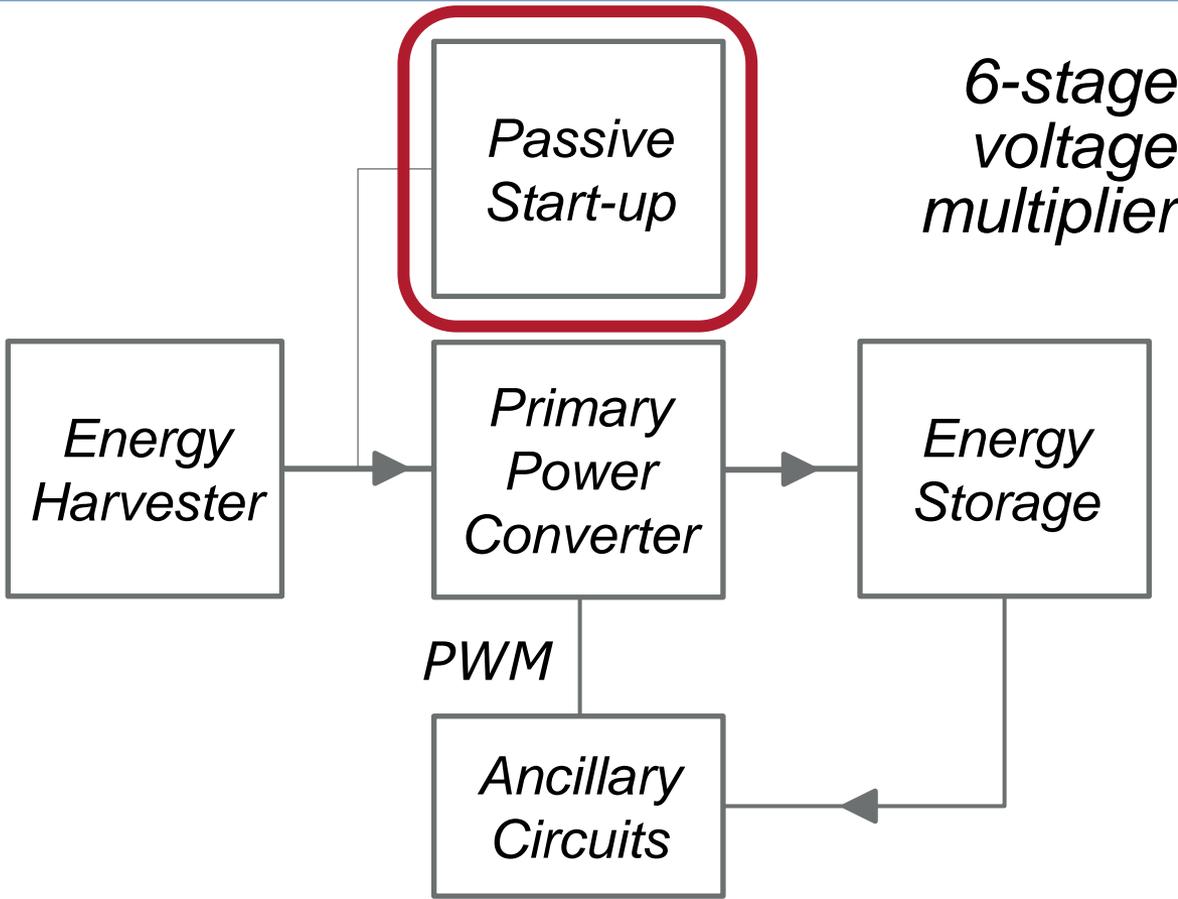
- Interface circuits and cold-start for electromagnetic harvester
- Implements MPPT through duty cycle control, altering the input impedance
- The MPPT cannot start from cold, some energy must be collected first
- Passive start-up-> active when running
- Power overhead of around 10-20 μ W when running

Low Power Implementation



- 88 Hz alternating boost converters
- One switch at 30 kHz
- Requires polarity detection

Imperial College
Low-power
implementation

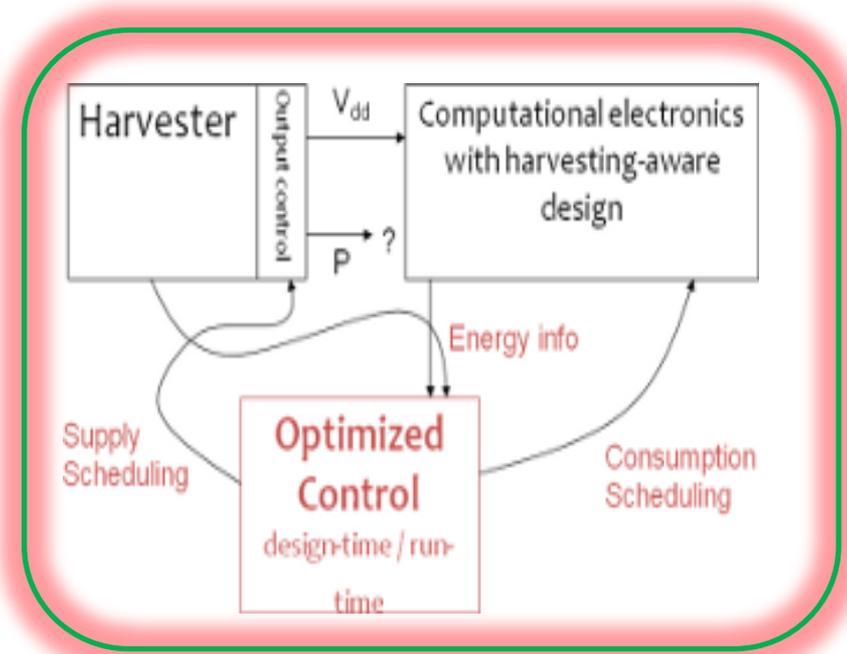


- *Voltage detector power-gates the μ C*
- *μ C controls activation of ancillary circuits and isolates voltage multiplier via JFET isolation switches*

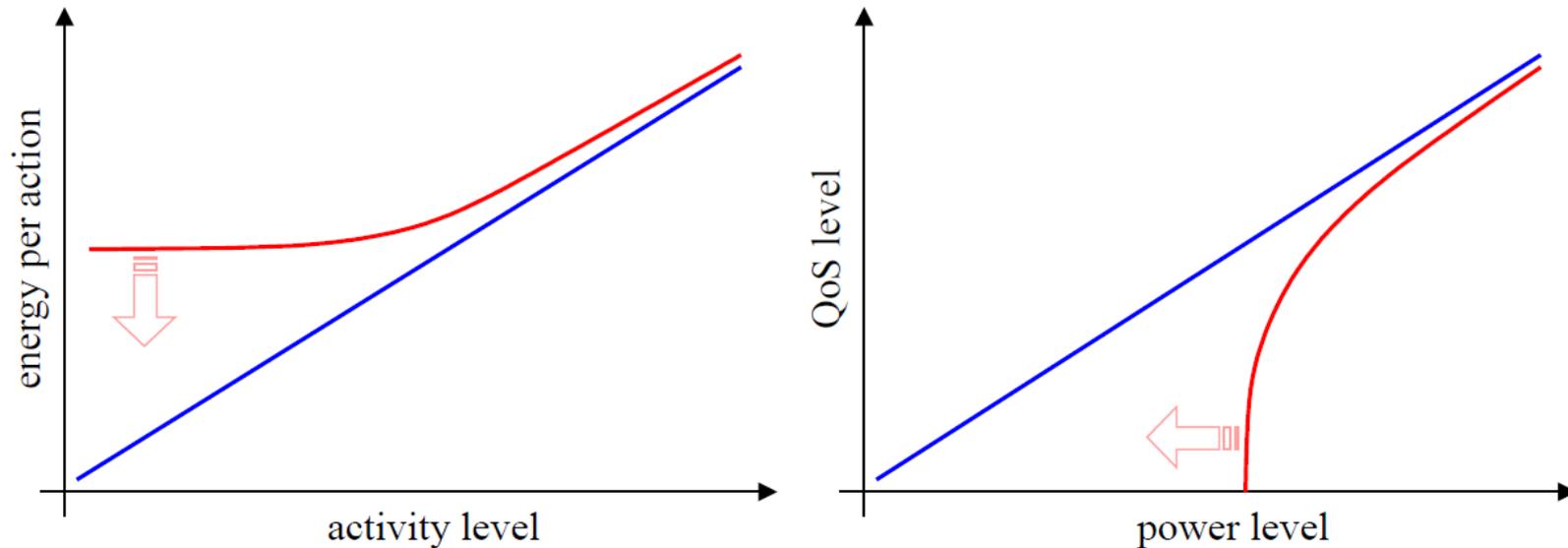
Energy Modulated Computation

Vision, aims and objectives

- Energy harvester aware design methods for computational logic
- Capable of working **under variable and unpredictable energy supply**
- **Circuit solutions for power control** and management techniques
- **Highly adaptive** computational circuits



Power Proportional Computing - limits



- ideal design
- real design

A. Yakovlev, *Energy-Modulated Computing*, Proc. DATE'11, Grenoble, March 2011, EDAA, pp. 1340-1345 (2011).

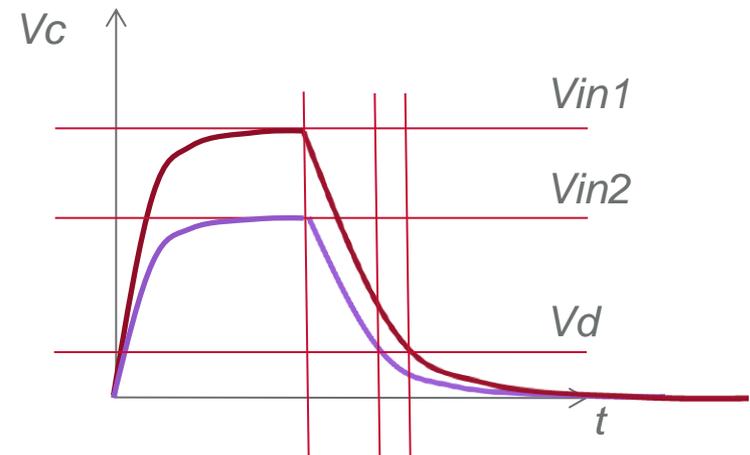
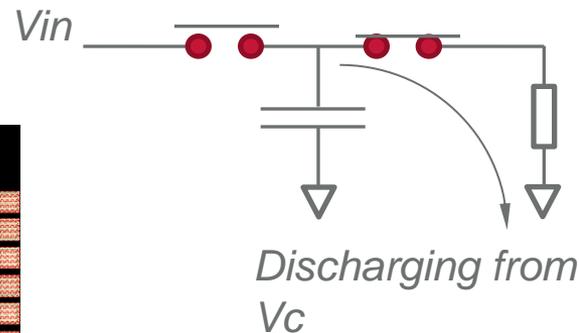
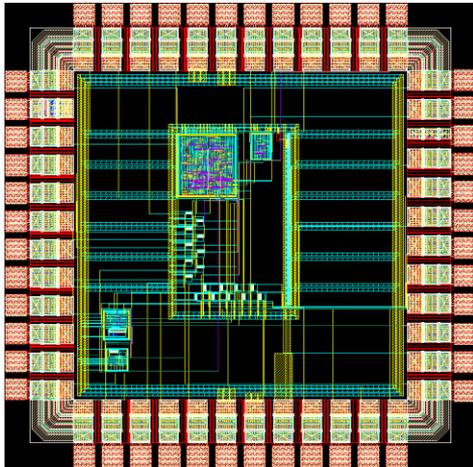
F. Xia, A. Mokhov, Y. Zhou, Y. Chen, I. Mitrani, D. Shang, D., Sokolov, A. Yakovlev, *Towards power-elastic systems through concurrency management*, IET Computers and Digital Technics, Vol.6, Iss. 1, pp.33-42, 2012.

Let's have a look at a circuit building block that came out of this project

Charge-to-Digital Converter

Discharging until a certain V_d in order to get rid of timing reference

Voltage sensor chip: UMC
CMOS 180nm

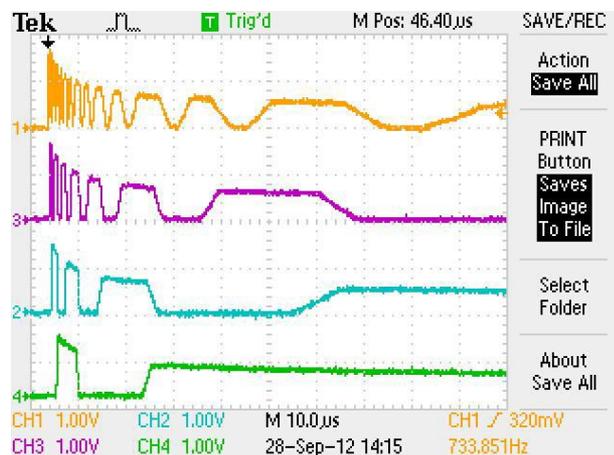


V_d is still a constant reference! But it does not have to be externally sourced. It could be based on some internal semiconductor characteristics

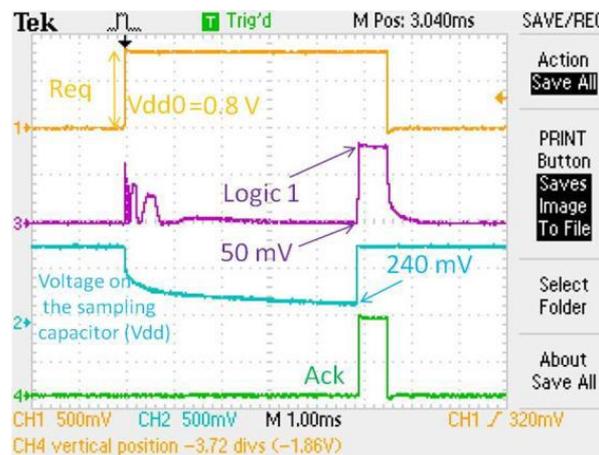
R. Ramezani, A. Yakovlev, F. Xia, J. Murphy D. Shang, "Voltage Sensing Using an Asynchronous Charge-to-Digital Converter for Energy-Autonomous Environments", IEEE Journal on Emerging and Selected Topics in Circuits and Systems (JETCAS), [in press].

Voltage sensor chip results

Counting action:

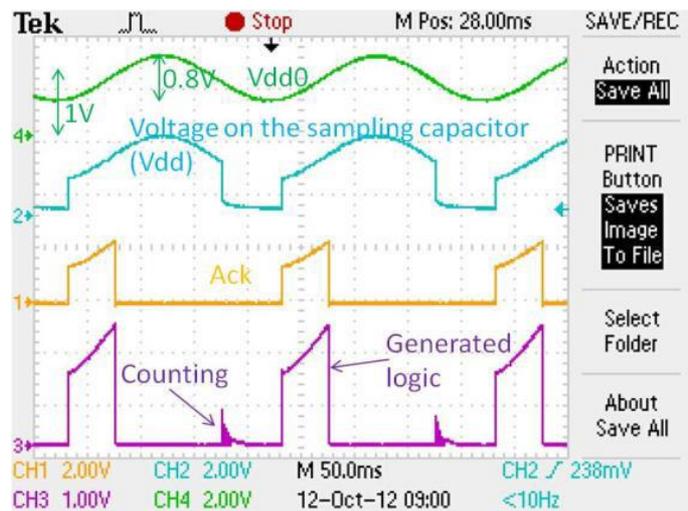


Reading the output:

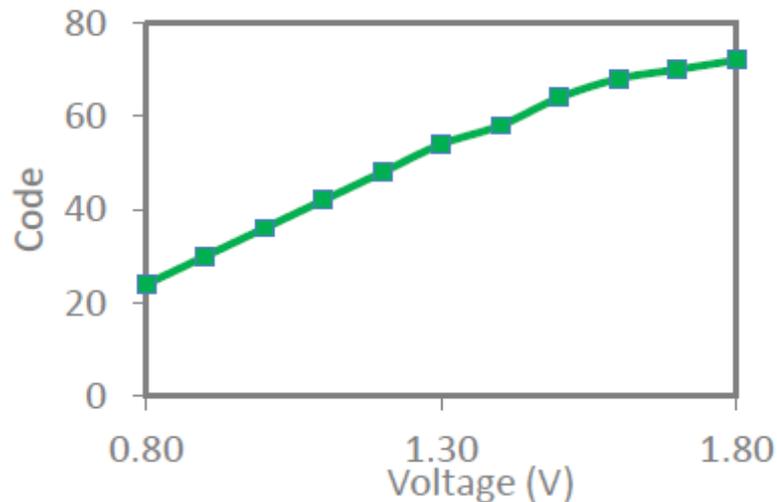


Information from
Prof Alex Yakovlev

Sensor operation under variable voltage:



Output code in the counter:



System Modelling

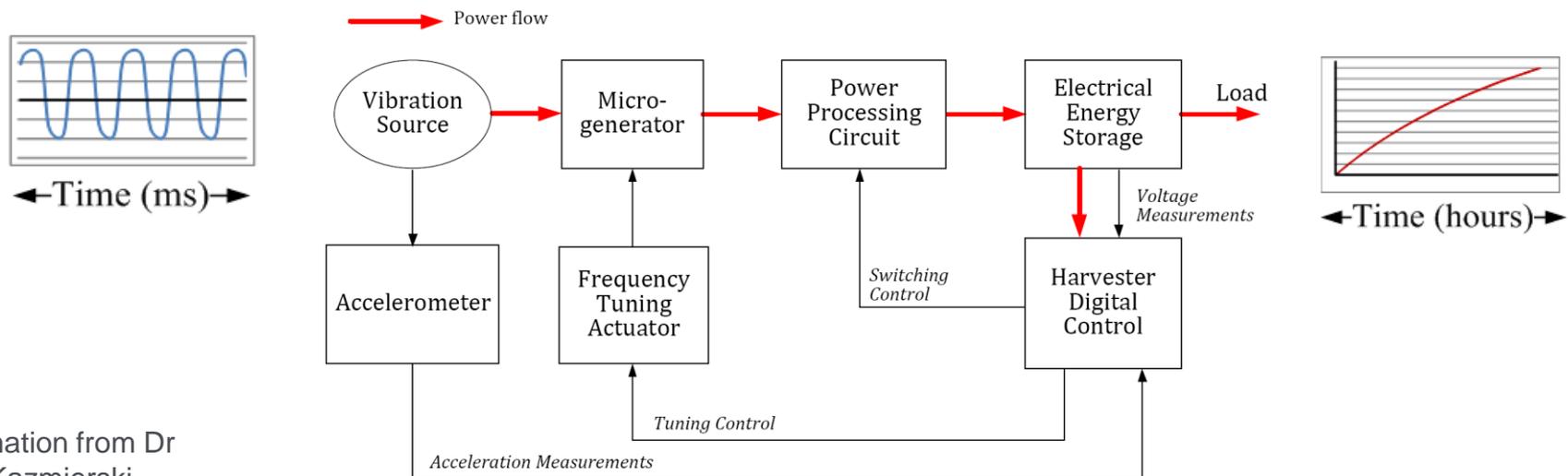
Why EH simulations are CPU intensive

Excessive CPU times due to disparate time scales

- High-speed microgenerator: small simulation time step (0.1ms)
- Low-speed storage: supercapacitor can take tens of hours to charge

Supercapacitor charging time is important

- It determines the system's duty cycle



Linearised State-Space Techniques Used

Existing state-of-the-art simulators use implicit equation formulation:

$$\mathbf{f}(\dot{\mathbf{x}}(t), \mathbf{x}(t), t); \quad \mathbf{x}(0) = \mathbf{x}_0$$

State equations:

$$\dot{\mathbf{x}}(t) = \mathbf{f}(\mathbf{x}(t), t); \quad \mathbf{x}(0) = \mathbf{x}_0$$

State equations can be solved very fast

- explicit march-in-time process
- no Newton-Raphson iterations.

However, explicit solution can be numerically unstable if step size is too large.

- *State-of-the-art SPICE-like simulators do not use it.*

Exploring the Complete Design Space

Even with accelerated simulation – it still takes too long to optimise an EH system by multiple simulations

- A complicated system which has many parameters that can affect the system performance
- There are trade-offs between increasing and decreasing each of the parameters, energy generation vs. energy consumption

Utilised technique

- RSM model for fast design space exploration
- Optimisation of the RSM model using MATLAB
- Combination of the power of HDL in modelling multi-domain systems and the power of MATLAB in computation

Simulation Times

Comparison of CPU times

Two order of magnitude acceleration

	Existing technique		Proposed technique
HDL	VHDL-AMS	SystemC-A	SystemC-A
Integration method	Newton-Raphson based	Newton-Raphson based	Linearised state-space
CPU time for Scenario 1	2185 sec	2386	20.3 sec
CPU time for Scenario 2	7 hours	8 hours	228 sec

Simulation Tool GUI

RSM Design Explorer

File Edit Help

Performance estimator of wireless sensor powered by kinetic energy harvester

Back

Diode bridge
4-stage voltage multiplier
Switching boost converter

Generated Power: 10.91 mW

Power Consumption: 1.41 mW

SuperCap Voltage: 2.70 V

Micro-generator

magnets

cantilever

coil

Power Processing

Energy Storage

Sensor Node

For the given input vibration amplitude and frequency

Estimated Number of Transmissions: 6565 /min

Transmission duty cycle depends on supercap voltage(V_c) and threshold voltage(V_{th}):

- $V_c < 2V$, no transmission
- $2 < V_c < V_{th}$, transmit every 1 min
- $V_{th} < V_c < 3.5$, transmit every 1 sec
- $V_c > 3.5$, transmit every 3ms

Max Displacement: 7.48 mm

Transfer Efficiency: 87.10 %

User parameters

Peak Amp: 700 mg (100~1000mg)

Freq: 50.00 Hz (50~250Hz)

Proof mass: 2.0 g (2~12g)

Number of coil turns: 2000 (500~5000)

Mechanical Q: 200 (100~500)

Cantilever

- Length: 10.00 mm
- Width: 2.00 mm
- Thickness: 150.0 um
- Material: Copper

Resonant Frequency: 50.01 Hz

Operating Freq Range: 49.750 to 50.250 Hz

Super-capacitor value (0.1~1F): 0.55 F

Energy consumption per transmission(10~1000uJ): 116.0 uJ

SuperCap threshold voltage (2.5~3V): 2.50 V

The resonant frequency of cantilever is close to the input frequency. Performance indicators updated.

Conclusions

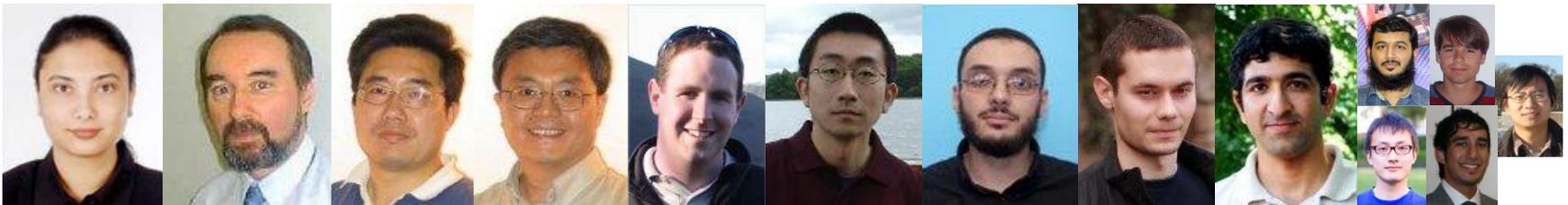
- Adaptive Harvesters
 - » MEMS VRD
 - » Magnetic potential well
- Power Electronics
 - » Optimal damping for piezoelectrics (SSPB)
 - » Optimal damping for electromagnetic harvesters (boost rectifier)
 - » Passive startup, and very low power overhead
- Energy Modulated Computing
 - » Asynchronous techniques
 - » Charge-to-digital converter
- System Modeling and Simulation
 - » Linear state-space models
 - » Response surface models

Acknowledgements

12 Investigators



14 Researchers



Acknowledgements

Work supported by EPSRC

Grant number EP/G070180/1

“Next Generation Energy-Harvesting
Electronics: Holistic Approach”

Eric Yeatman, Bernard Stark, Bashir Al-Hasmimi, Tom Kazmierski, Alex Yakovlev, Geoff Merritt, Anisha Mukherjee, Steve Wright, Alex Weddell, Plamen Proynov, Gyorgy Szarka and all those involved in the project

<http://www.holistic.ecs.soton.ac.uk>



2013
PowerMEMS
United Kingdom, Dec 3rd – 6th 2013

PowerMEMS School Dec 2nd – 3rd

More information:

<http://www.powermems2013.org>

Join our Facebook Page:

<http://www.facebook.com/PowerMEMS2013>