



# Advancing the performance of energy harvesting for structural health monitoring

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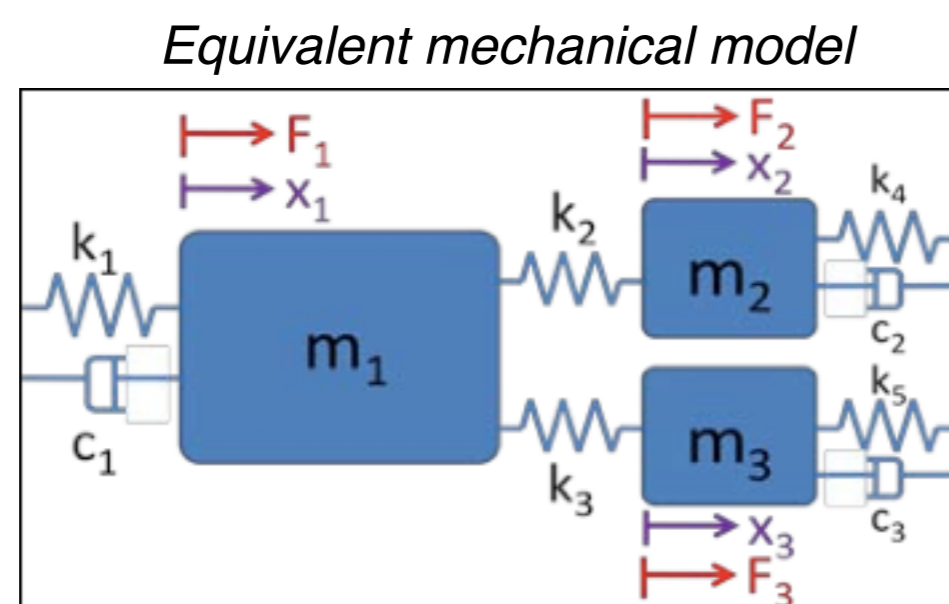
## A multi-degree-of-freedom electrostatic energy harvester

**Problem targeted:** Narrow operational frequency band.

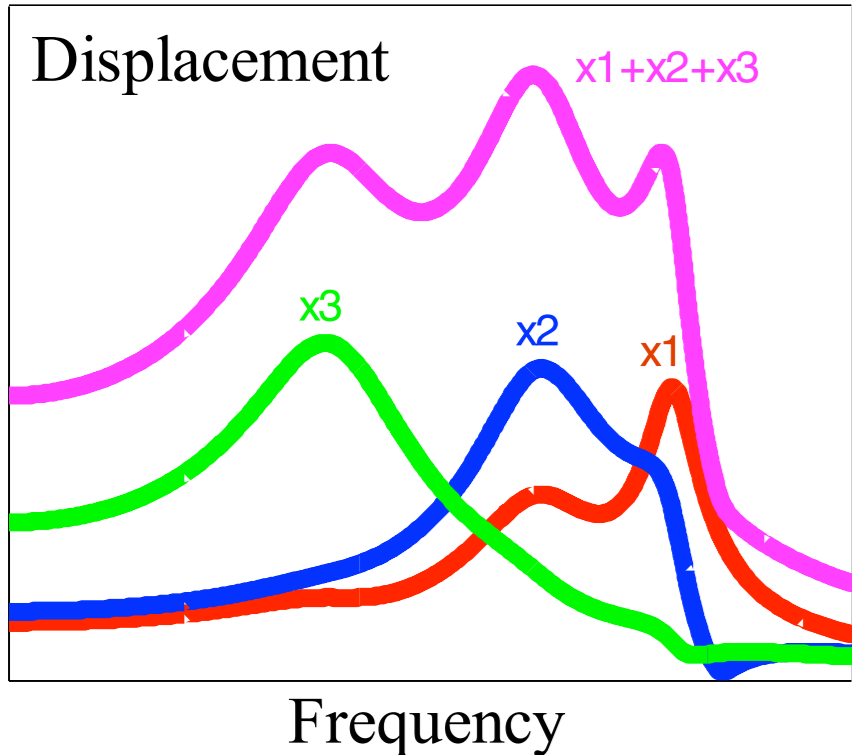
**Proposed solution:** With  $n$  number of proof mass, the system would have  $n$  number of resonant frequencies. Through designing the parameters: mass  $m$ , spring stiffness  $k$  and damping coefficient  $c$ , the resonant peaks can be placed closely to each other. Hence, a quasi-broadband effect can be achieved.

This design technique can be used to potentially increase the operational frequency bandwidth and amplifying the peak displacement.

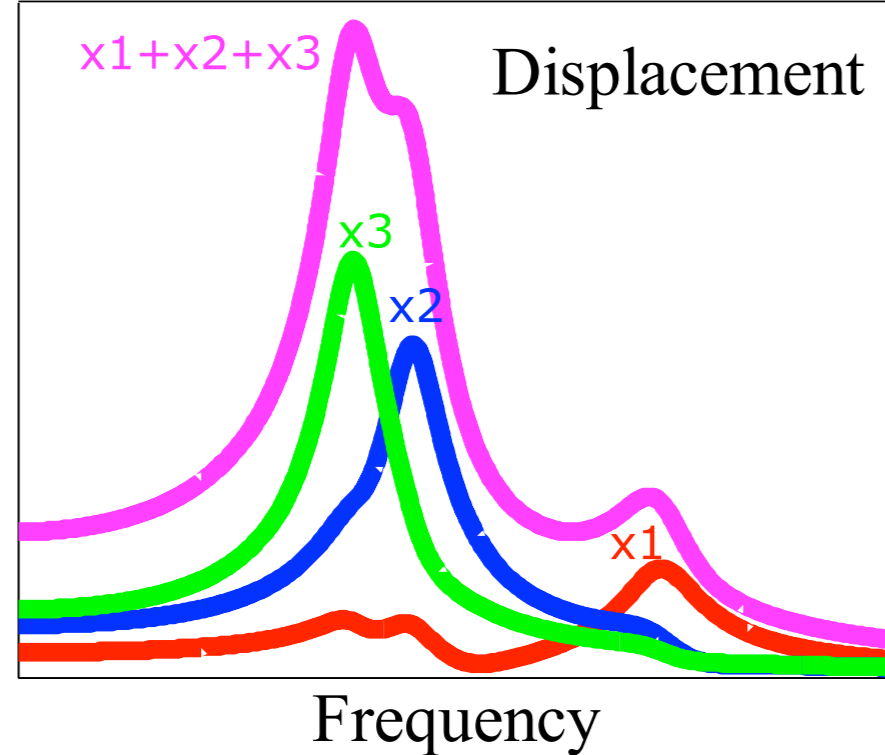
Governing equation:  
 $[M]\ddot{X} + [C]\dot{X} + [K]X = F$



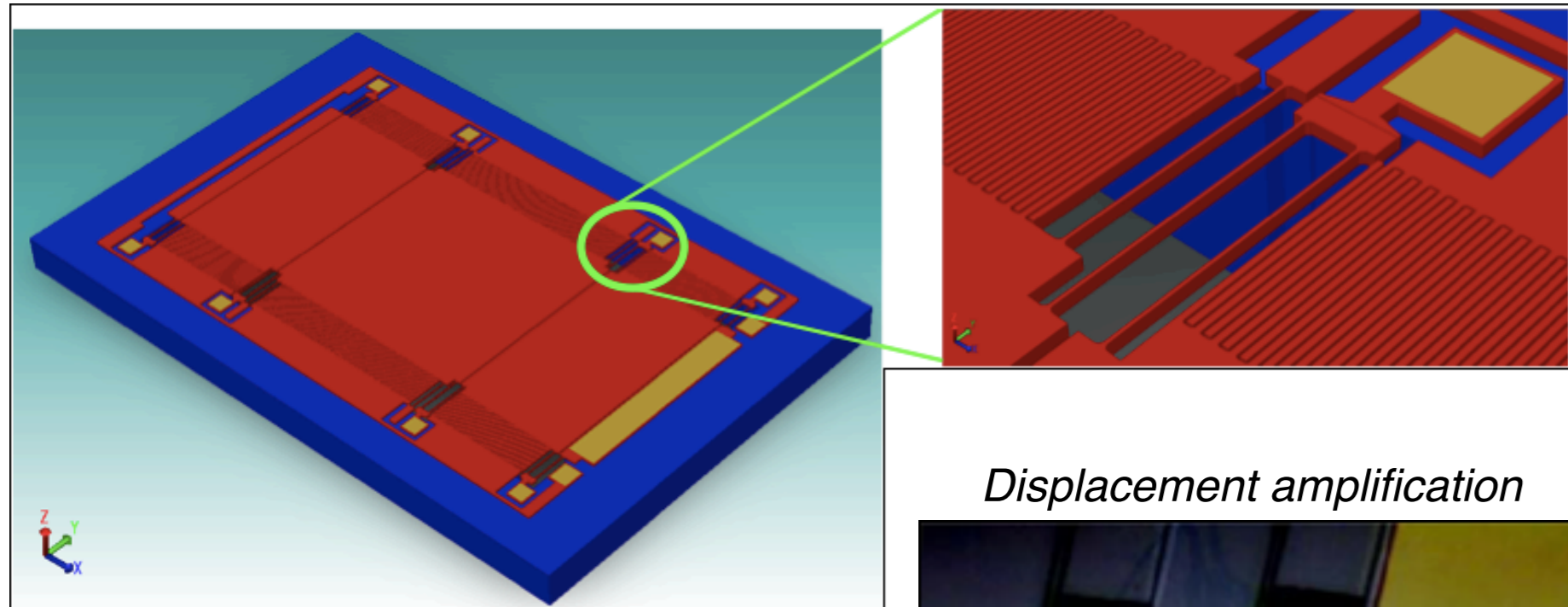
Increasing frequency bandwidth



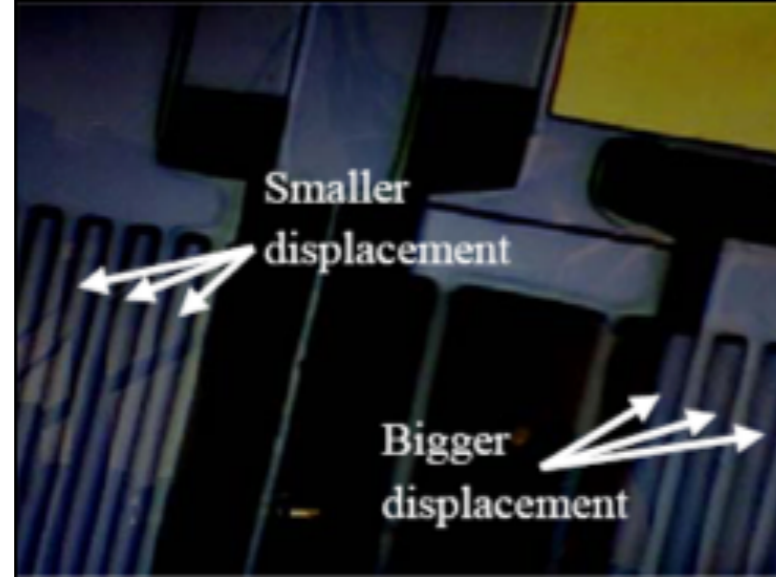
Increasing displacement



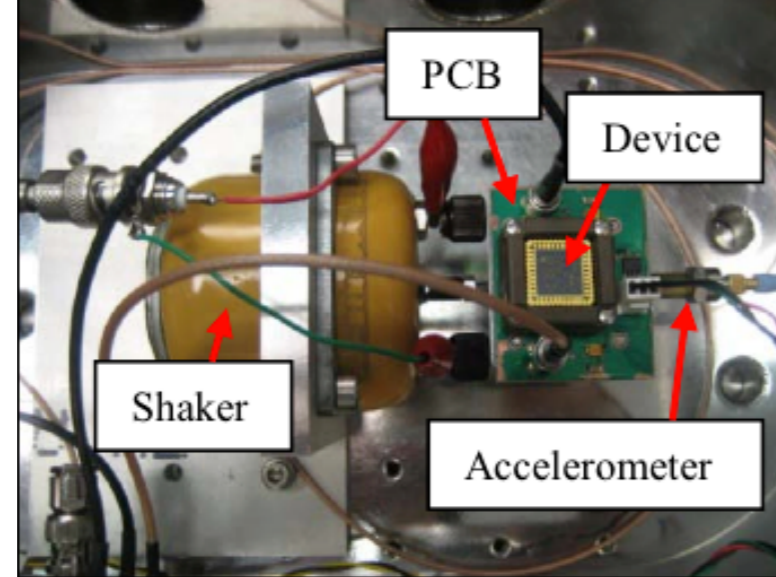
3D view of the designed 3 degree-of-freedom MEMS energy harvester



Displacement amplification



Experimental test setup



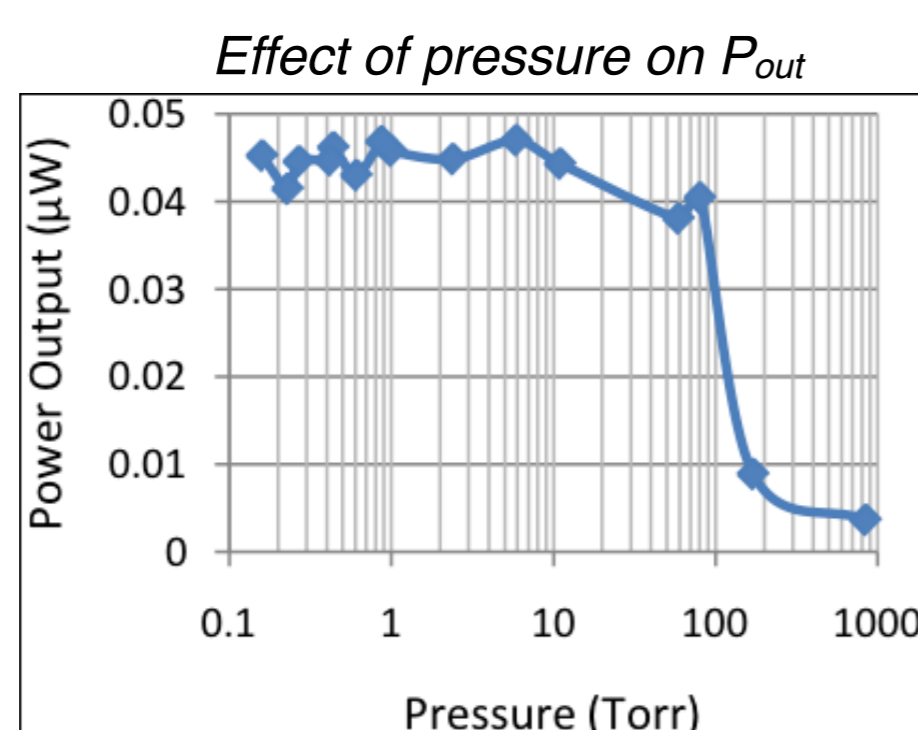
### Method:

3-degree-of-freedom MEMS-based electrostatic energy harvester was fabricated using the standard SOI-MUMPS process. Testing and characterisation of devices at first resonant mode was carried out both in air and in vacuum.

### Result:

The maximum measured power output from the current device is  $0.076 \mu\text{W}$  with peak voltage of  $0.88 \text{ V}$ , frequency of  $14 \text{ kHz}$ , input acceleration of  $1.53 \text{ ms}^{-2}$  and external load of  $5.1 \text{ M}\Omega$ .

Power output  $P_{out}$  is directly proportional to the square of input acceleration and bias voltage. In terms of effect from pressure, there is a threshold below which the damping begins to drastically diminish. Thus, enabling larger vibration amplitudes.



Comparing the current device with selected electrostatic harvesters

Reference	Frequency (Hz)	Power ( $\mu\text{W}$ )	Power/Mass/Acceleration ( $\mu\text{W/g/ms}^{-2}$ )
Tashiro (2002)	6	36	0.046
Mitcheson (2004)	30	3.7	0.74
Arakawa (2004)	10	6	2.37
Despesse (2005)	50	1052	1.15
Ma (2005)	4200	0.065	0.42
Chiu (2007)	1870	1.2	1.85
This device (in air)	1400	0.017	13.16
This device (in vacuum)	1430	0.113	87.97

## Literature cited

- Wong, Z.J., Yan, J., Soga, K. and Seshia, A.A., (2009), A multi-degree-of-freedom electrostatic MEMS power harvester, *Proceedings of 9th International Workshop on Micro- and Nanotechnology for Power Generation and Energy Conversion Applications (PowerMEMS 2009)*, 1-4 Dec, Washington DC, USA, pp. 300-303.
- Ye, G., Yan, J., Wong, Z.J., Soga, K and Seshia, A.A., (2009), Optimisation of a piezoelectric system for energy harvesting from traffic vibrations, *Proceedings of IEEE International Ultrasonics Symposium (IUS)*, 20-23 Sept, Rome, pp. 759-762
- Ye, G. and Soga, K., (2011), Energy harvesting from water distribution systems, Department of Engineering, University of Cambridge, 30pp. (to be published)

## Introduction

**Motivation of energy harvesting:** To enable sustainable self powered wireless sensor networks for structural health monitoring.

### Ambient vibration harvesters:

- Suitable for integration into dark and enclosed systems.
- Vibration sources are ubiquitous. (The world is in a constant state of agitation.)

### Micro-Electro-mechanical Systems (MEMS):

- Size miniaturisation.
- Integration with ICs.
- Low cost (when mass produced).

### Issues:

- Narrow operational frequency band around resonance.
- Limited power density for feasible implementation.
- Lack of real vibration analytical models for system optimisation.
- Lack of studies on the feasibility in real world applications.

## Energy harvesting for water distribution systems

**Problem targeted:** Feasibility study of employing energy harvesting to provide sustainable power supply for inaccessible wireless sensor nodes in water distribution systems.

### Possible sources of energy:

- (1) Hydraulic energy in bypass pipes.
- (2) Hydrothermal energy in water-air temperature gradient.
- (3) Kinetic energy from water pressure fluctuation.

**Background research:** The power consumption of a typical wireless hydraulic sensor node is at the order of  $10$ 's  $\text{mW}$ . While solar cells can generate sufficient power, they are not suitable for enclosed applications. Ambient vibration energy harvesting from manhole cover, even after the optimisation using the genetic algorithm, was still not enough to power the sensors.

### (1) Hydraulic energy harvester:

Diverting water into bypass pipes to power microturbines. A pressure gradient is needed. Three designs were investigated.

Bypass systems	Power
(a) Release water to the environment	$144 - 196 \text{ W}$
(b) Flow driven by pressure drop after a valve	$0.07 - 0.32 \text{ mW}$
(c) Flow driven by a Pitot tube	$< 1 \mu\text{W}$

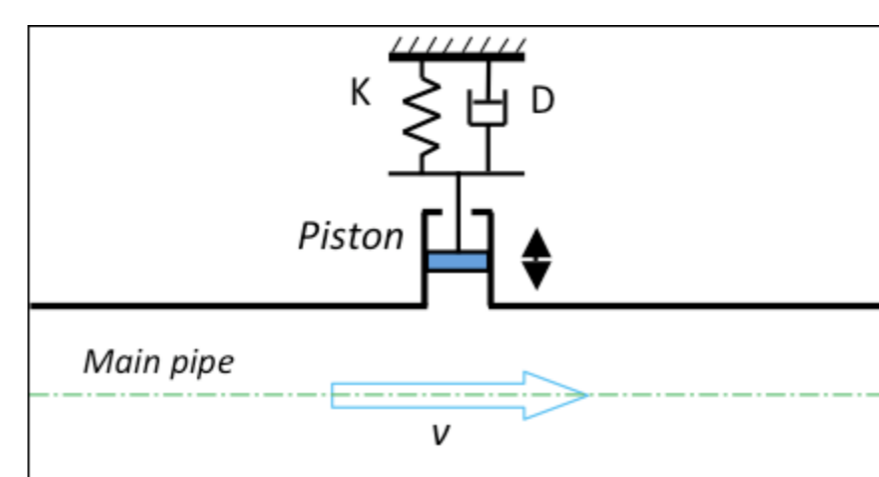
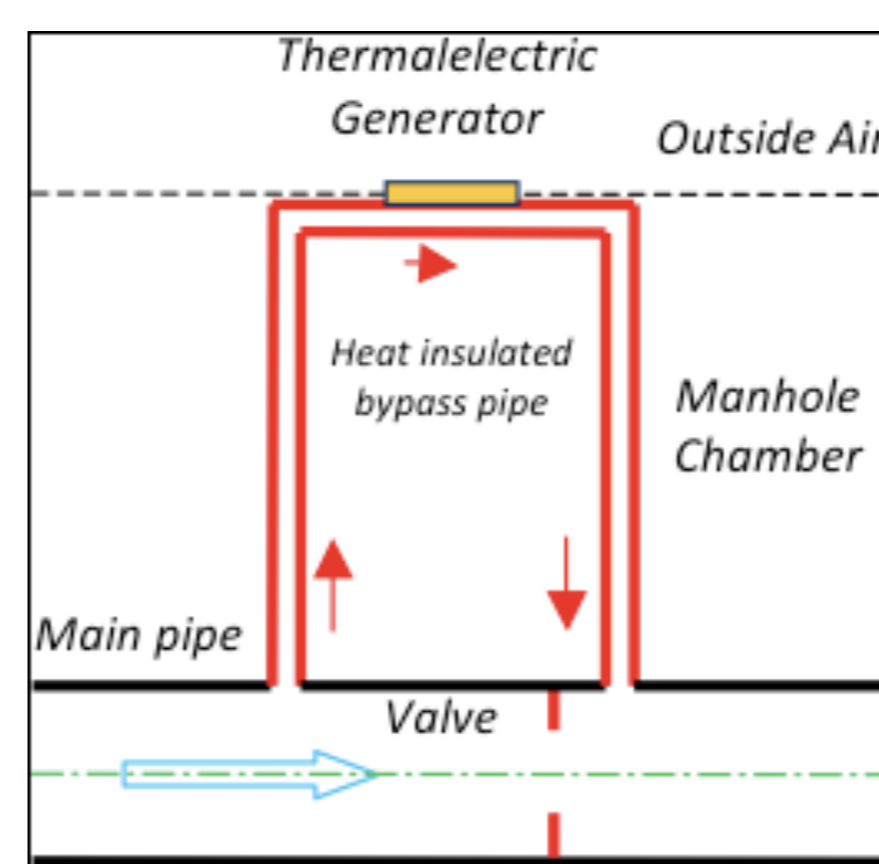
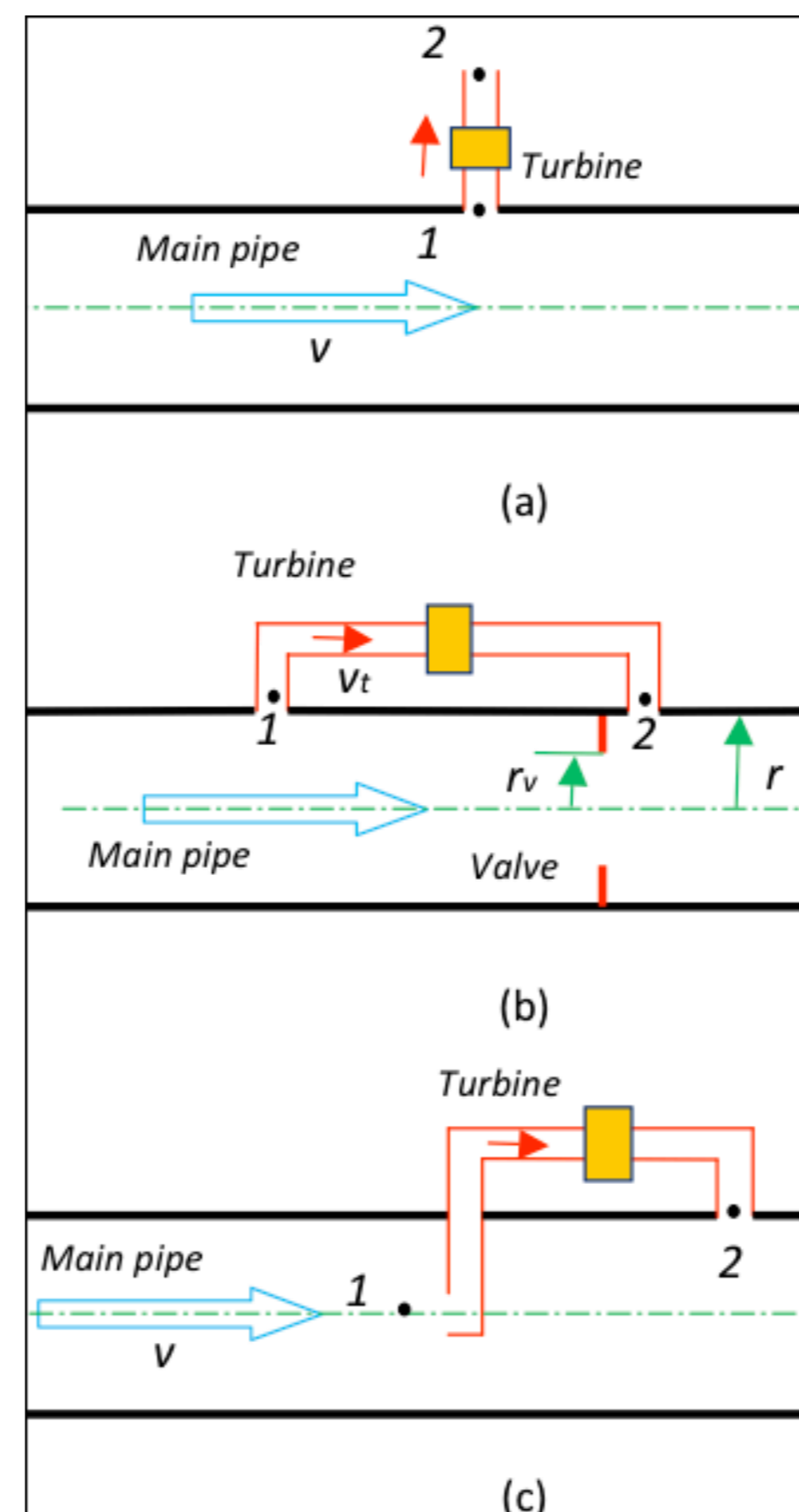
System (a) provides more than enough power. However, it wastes significant amount of water and causes severe disruption to the water distribution system. While (b) and (c) are inadequate to meet the power budget requirement.

### (2) Hydrothermal energy harvester:

A water bypass system was designed for this purpose (right). The mean water-air temperature gradient (North England) is around  $3^\circ\text{C}$ . Using this value, a thermoelectric generator of size  $40 \times 40 \times 4.2 \text{ mm}$  can generate about  $2.8 \text{ mW}$ . An array of these generators can meet the power requirement.

### (3) Water pressure fluctuation energy harvester:

An electro-mechanical system (right) was designed, which harvests the kinetic energy from pressure fluctuation in the main pipe.



Genetic Algorithm was employed to optimise the design parameters of the harvester for real pressure fluctuation data. Numerical model demonstrated that such a system could ideally produce several  $\text{mWcm}^{-2}$ .

**Conclusion:** A feasibility study utilising fundamental modelling and analysis was carried out. The hydrothermal and water pressure fluctuation energy harvesters appear to yield promising results. Future work will be focused on the experimental testing and further analysis of these two proposed systems.

## Acknowledgement

Research funding from the Engineering and Physical Sciences Research Council (EPSRC) for the Underground M3 project and the NEPTUNE project.

## Optimisation for real vibration sources

**Problem targeted:** Lack of analytical models to describe real vibration sources. Most researches simply employ sinusoidal time domain acceleration as vibration input.

**Proposed solution:** A genetic algorithm with numerical simulations that considers the effects of each parameter of the real vibration input to produce an optimal frequency response. A piezoelectric cantilever system was optimised for experimental acceleration data from the vibrations of a vehicle excited manhole.

### Modelling piezoelectric cantilever energy harvester:

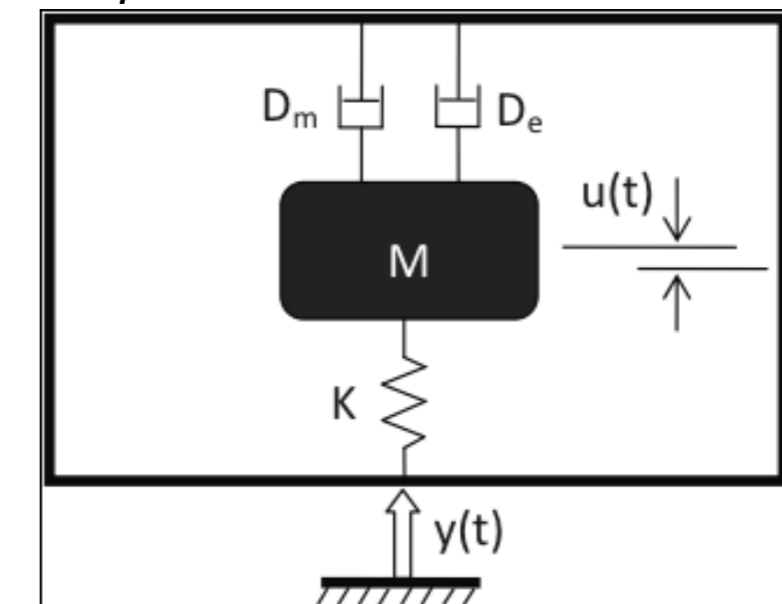
Equation (3) is  $M\ddot{u}(t) + D\dot{u}(t) + Ku(t) + Av(t) = -M\ddot{y}(t)$  (1)

the output power  $v(t) = RA\dot{u}(t) - RC\dot{v}(t)$  (2)

when the system operates at a specific resonant frequency.  $p = \frac{RM^2A^2\omega^4}{2[(A^2R + D)^2 + (RCD\omega)^2]}y^2$  (3)

However, real vibrations are broadband in nature.

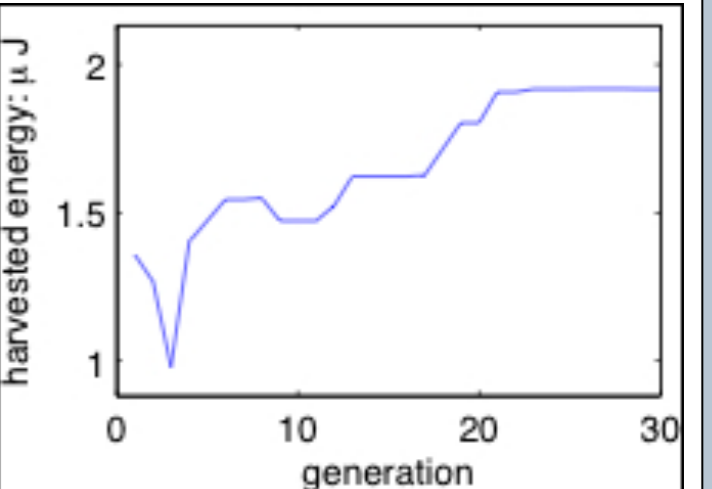
Equivalent mechanical model



$M$  - proof mass  
 $D_M$  - mechanical damping  
 $D_E$  - electrical damping  
 $D$  - total damping  
 $K$  - spring stiffness  
 $A$  - piezoelectric coefficient  
 $R$  - resistive load  
 $C$  - capacitance of piezoelectric material  
 $u(t)$  - displacement  
 $y(t)$  - excitation displacement  
 $v(t)$  - output voltage  
 $p$  - output power  
 $\omega$  - natural frequency

**Method:** Initially, a trial point is selected for each parameter and is then iteratively optimised. Roulette wheel selection is used to reproduce new generation of populations. Result converges to an optimum design with maximum energy output after  $n$ -generations.

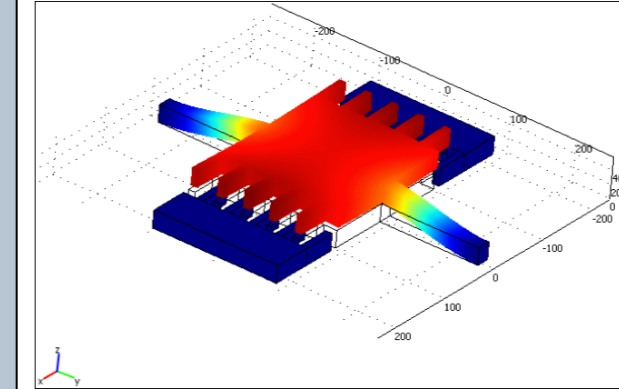
Power after n-generations



**Result:** Experimental testing has shown significant enhancement in energy harvested from the design optimised by the genetic algorithm than sinusoidal simulations. This technique is promising for optimising harvesters aimed at practical applications.

## Novel design improvements

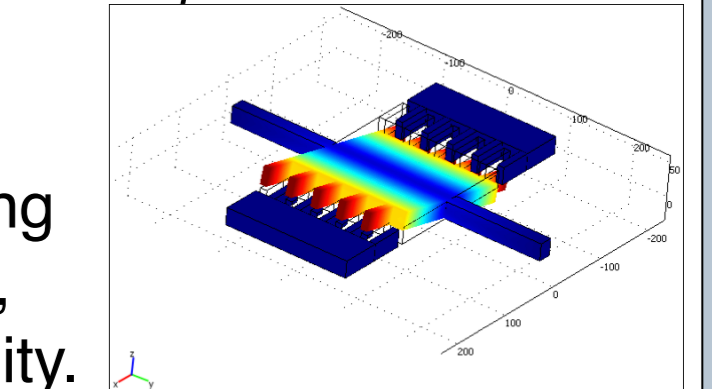
### Torsional vibration mode



### Advantages

- Large  $\Delta C$  without displacement limit.
- Allow compact placing of comb fingers. Thus, increases power density.

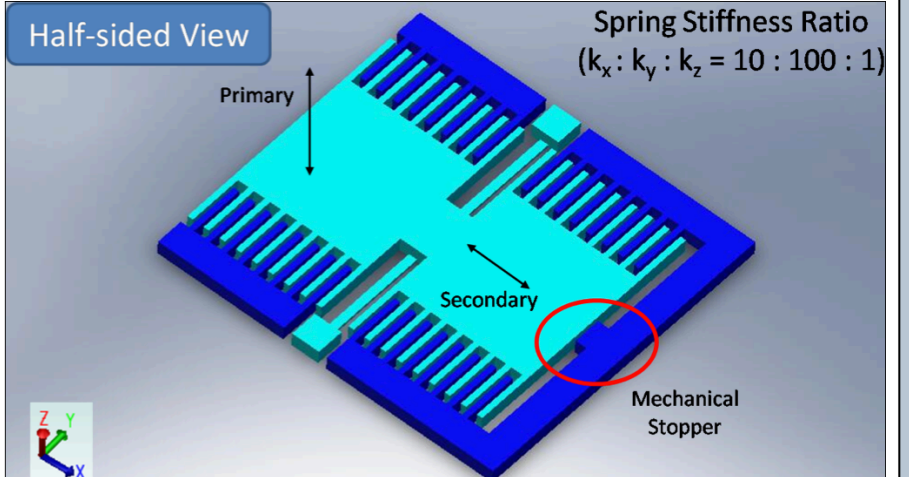
### Out-of-plane vibration mode



### Advantages

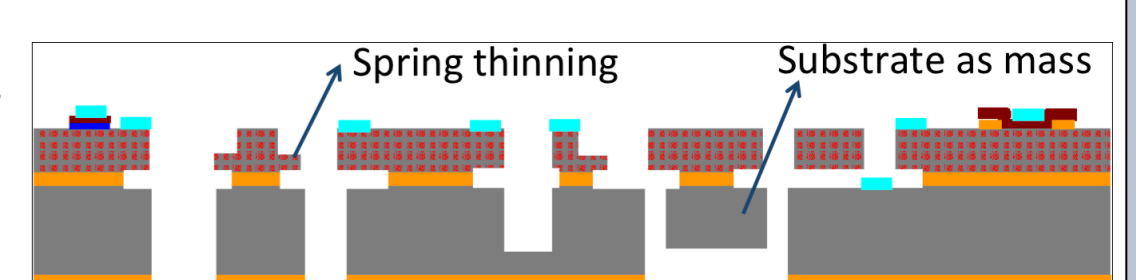
- Simultaneous energy harvesting in  $x$  and  $z$  directions.
- Mechanical stopper to limit unexpectedly large vibration in real-world engineering structures.

### Two-axis vibration power harvester



## Development of new micro-fabrication process on SOI wafer

(collaboration with National Research Council, Italy)



- To fabricate more complicated structures for higher performance.
- To enable device & circuits integration.

## Future work

- MEMS design improvement.
- Investigate novel methods to maximise the power density and increase operational bandwidth.
  - Wide band
  - Random vibration
  - Mechanical amplifier
  - Multi-axial
  - Coupled harvesters
- Device design for various energy sources and real applications.
- Power circuit design and system integration.
- Test equipment setup to model real vibrations.

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