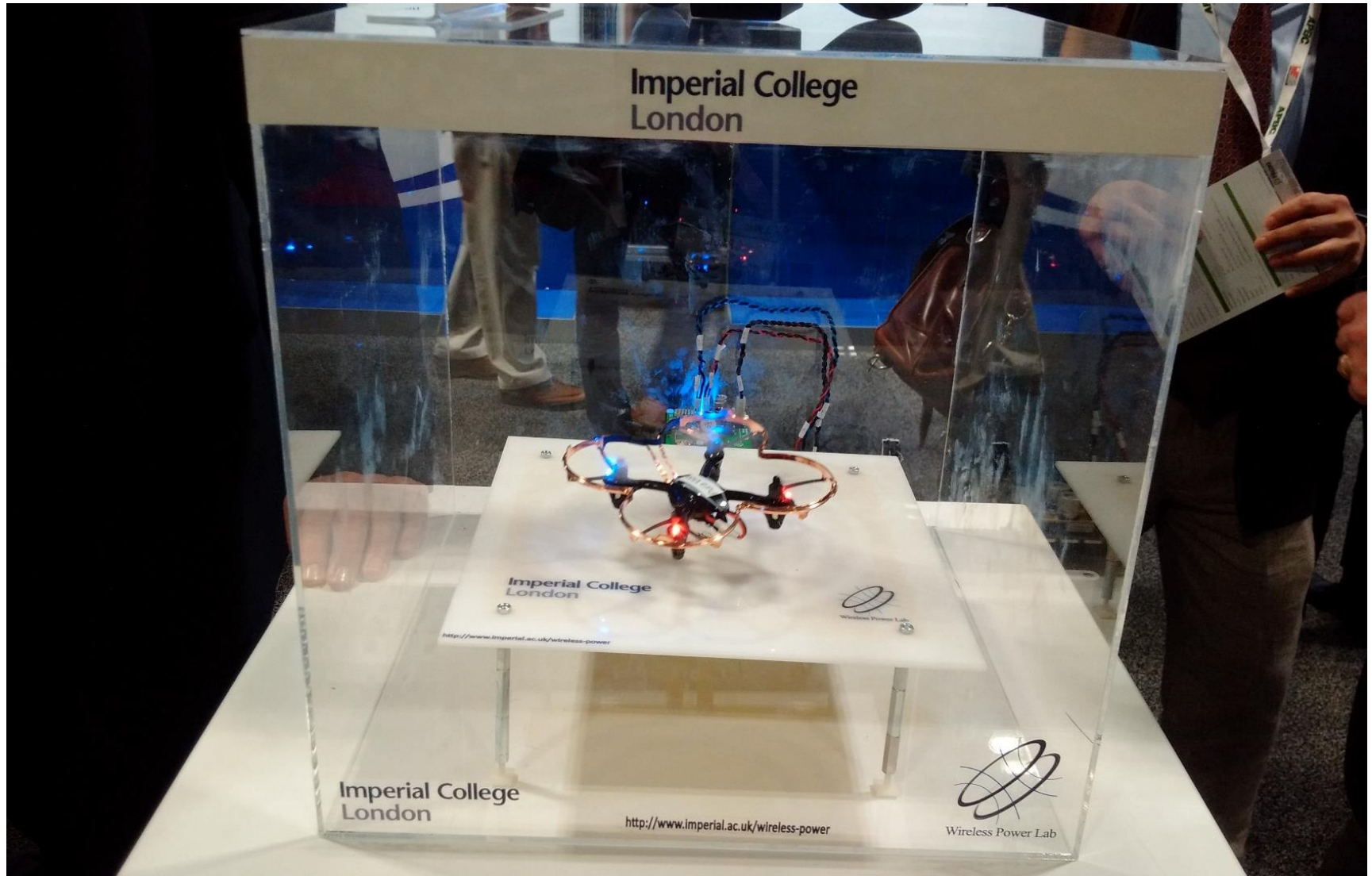
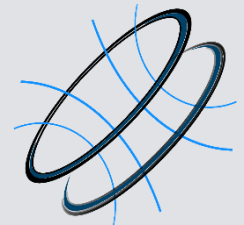


Inductive Power Transfer in the MHz ISM bands: Drones without batteries

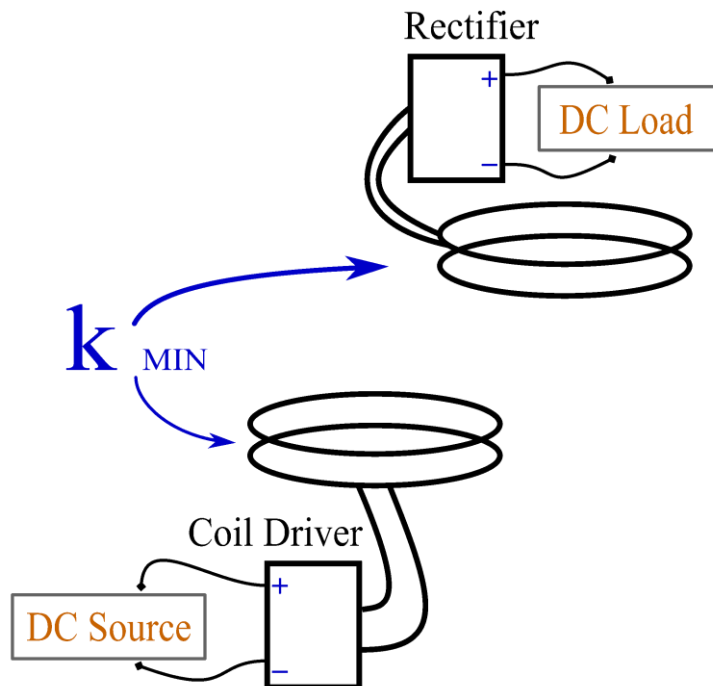
**Paul D. Mitcheson, S. Aldhafer, Juan M. Arteaga, G. Kkelis and
D. C. Yates**

EH2017, Manchester

The Concept

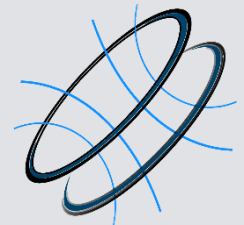


Challenges for Drone Charging



Dynamic system challenges:

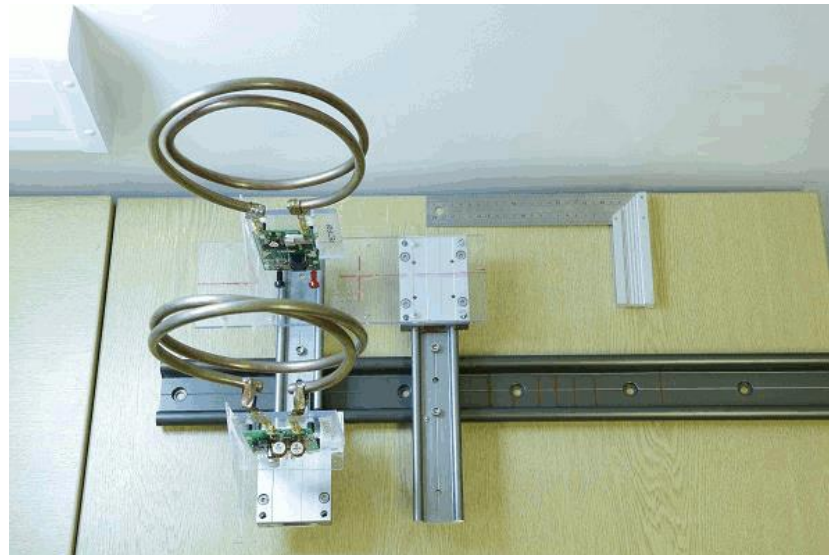
1. Light weight system
2. High link efficiency capability independent of k
3. Optimal reflected load with varying k
4. High efficiency of the inverter and rectifier with varying k and varying power throughput



Overview

- Light weight system and high link efficiency capability independent of k
- Optimal reflected load with varying k
- High efficiency of the inverter and rectifier with varying k and varying power throughput
- Demo video
- Conclusions

Light Weight and Link Efficiency Capability



Commercial systems: Automotive and phones

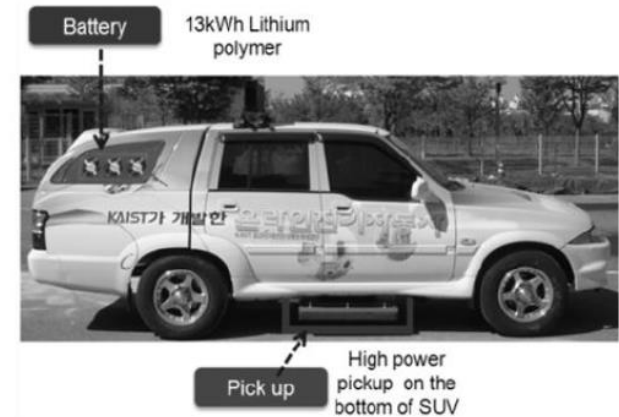
Most use ferrite to enhance coupling: too heavy

Witricity EV charger

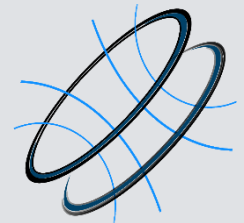
- RX ~10 kg, TX ~30 kg, 85 kHz

Qualcomm Halo

- 20 kW, 20 kg, 20kHz



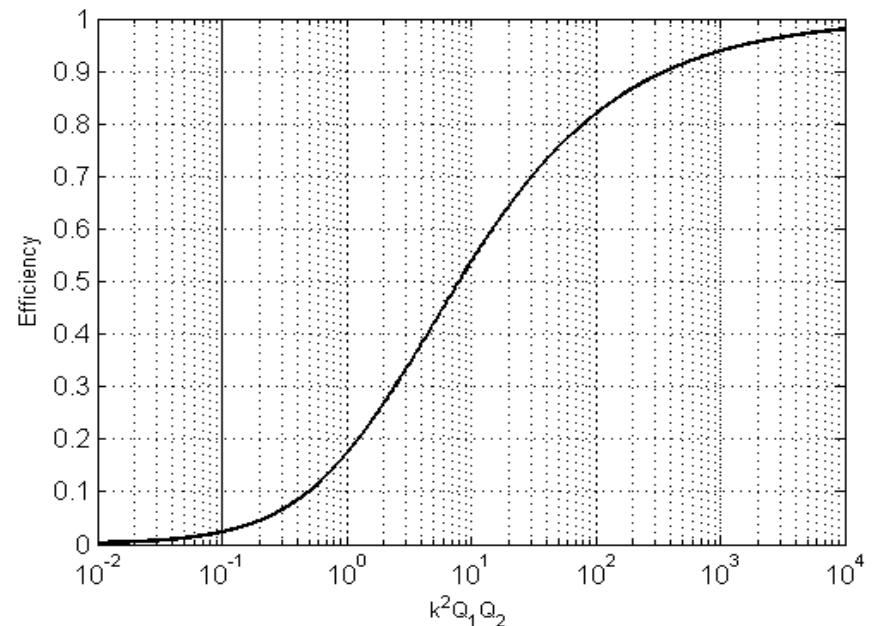
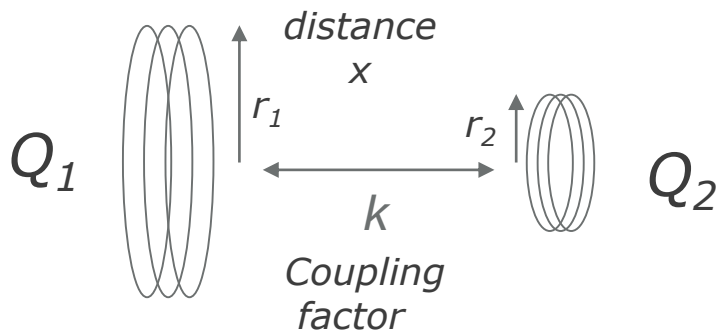
- Qi standard very short range
- Limited power levels



Reliance on High Q, not high k

Efficiency given by:
$$\eta = \frac{k^2 Q_1 Q_2}{\left(1 + \sqrt{1 + k^2 Q_1 Q_2}\right)^2}$$

*Secondary resonance
Optimal load*



Need to maximise $k^2 Q_1 Q_2$

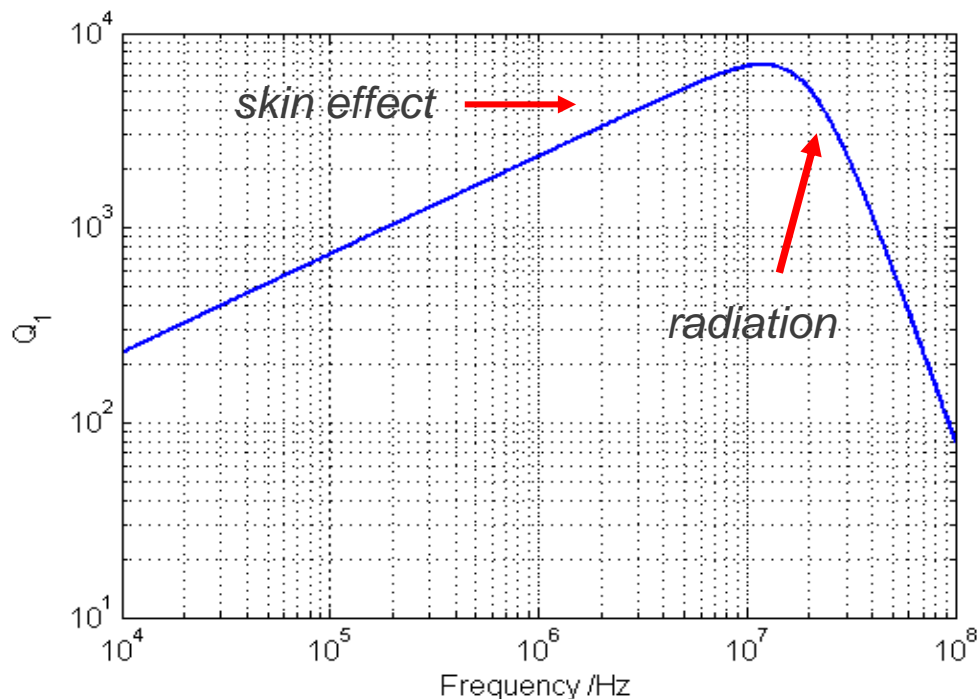
$k^2 Q_1 Q_2 > 10$ for $\eta > 50\%$

$k^2 Q_1 Q_2 > 350$ for $\eta > 90\%$

High Frequency is Key

Efficiency given by:
$$\eta = \frac{k^2 Q_1 Q_2}{\left(1 + \sqrt{1 + k^2 Q_1 Q_2}\right)^2}$$

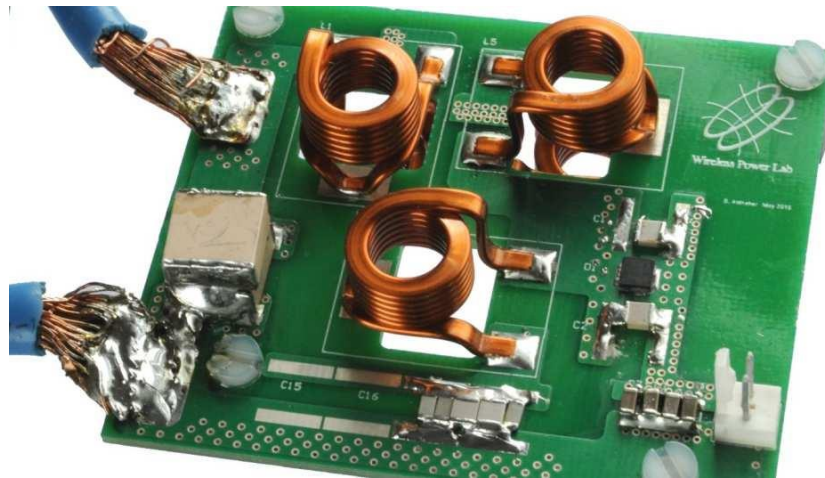
*Secondary resonance
Optimal load*

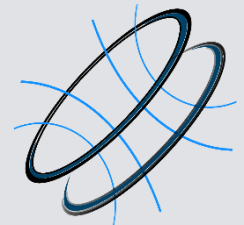


- High frequency (MHz) allows high Q
- High frequency allows removal of ferrite
- Skin effect allows very thin conductors

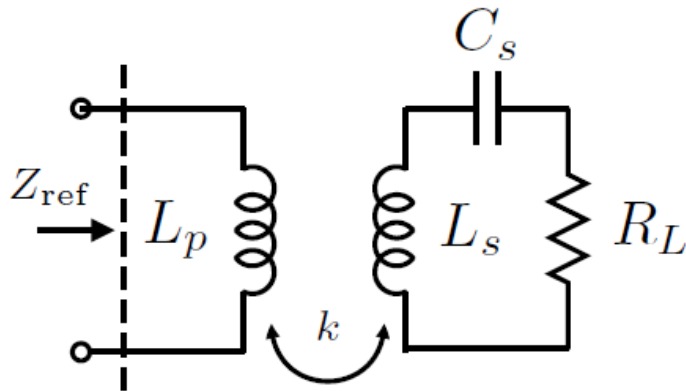
Light weight and varying k capability are possible with high frequency, high Q coils

Optimal Reflected Load

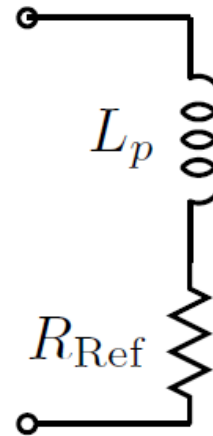




Inductive Link Properties – varying R_L and varying k



(a) ideal circuit representation



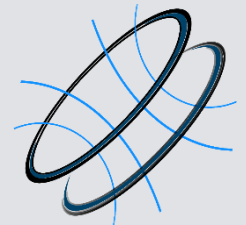
(b) equivalent circuit

$$Z_{ref} = \frac{\omega^2 M^2}{R_L + jX_{Ls} - jX_{Cs}}$$

$$Z_{ref} = R_{ref} = \frac{\omega^2 M^2}{R_L}$$

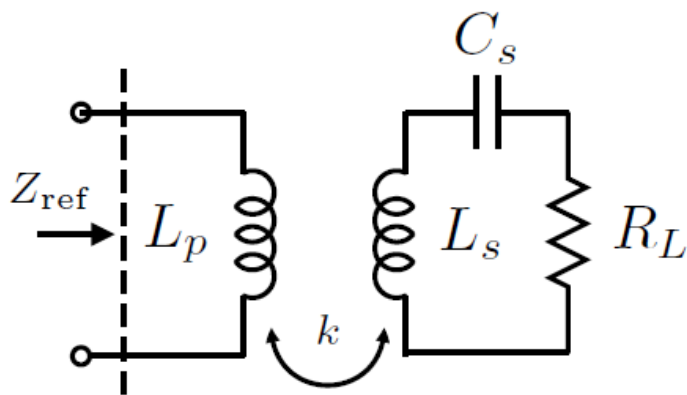
- Purely real across all values of values of R_L and k with secondary resonance.
- Reflected reactance
 - Cause detuning of inverter – and transmit current rapidly drops
 - Inefficient to transfer reactive power across link

Not true for parallel secondary resonance: hence we choose series compensation

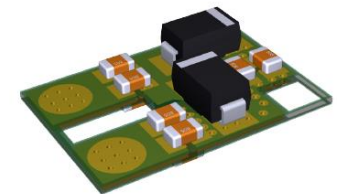
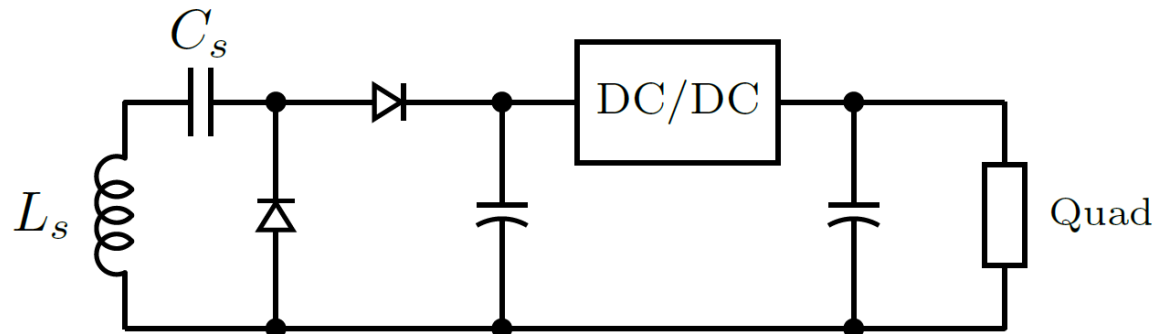


Rectifier's effect on reflected load

- The previous analysis is only valid if the rectifier has resistive input impedance.

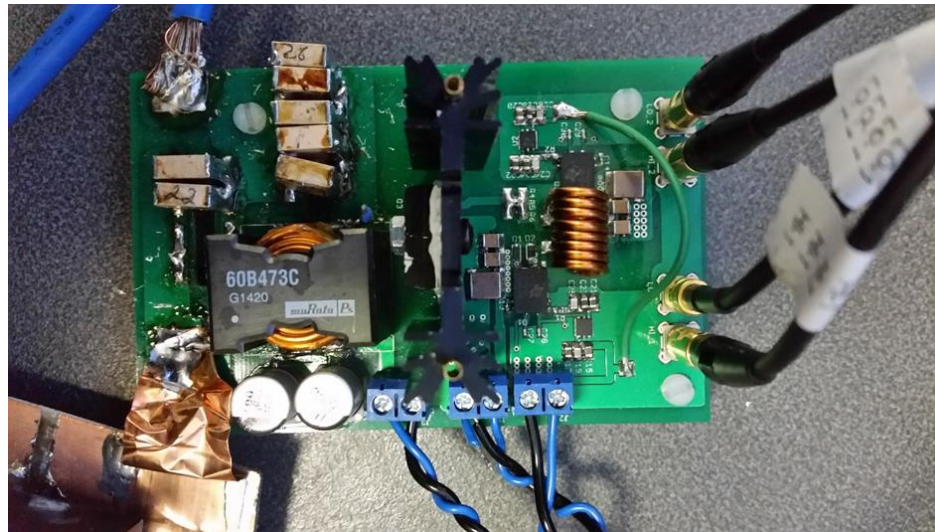


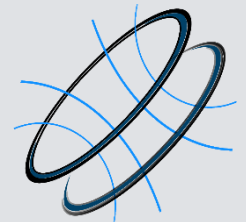
- The class-D rectifier is current source driven (suitable for a series tuned secondary)
- The class-D rectifier presents a purely real load on the series tuned circuit, independent of its DC load



"sim card"
rectifier

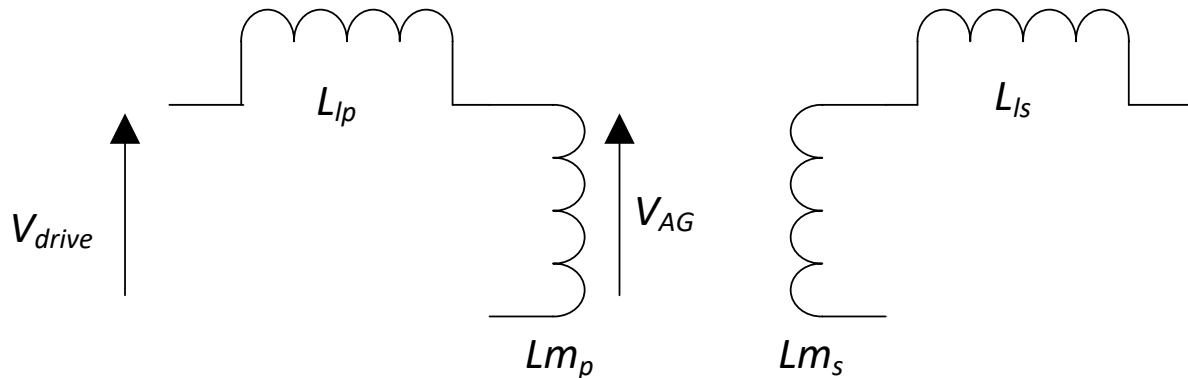
High Efficiency with Varying k and R





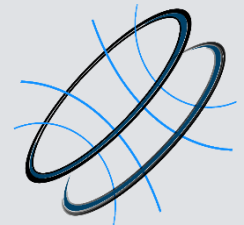
Requirements to drive the link

- Poor power factor unless leakage inductances are resonated out – because coupling factor typically $< 10\%$
- Only a fraction of the applied voltage is seen at air gap voltage



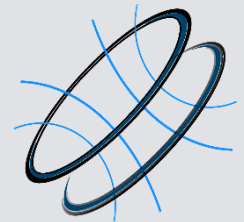
- Traditional to resonate out primary inductance to reduce VA rating of drive circuit

Common misconception: poor coupling factor = poor efficiency



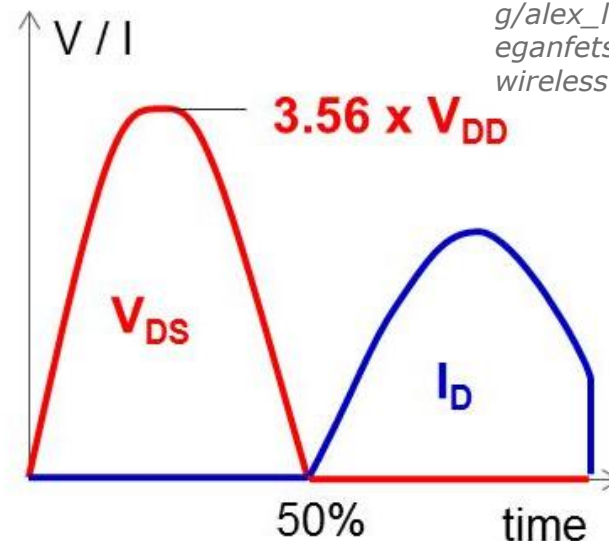
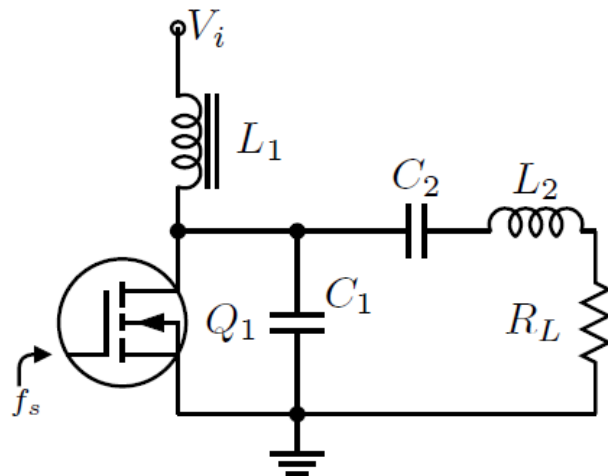
Inverters

- Conventional hard-switching not suitable in MHz region
 - Device switching times become comparable to driving signal period
 - Can be inefficient at higher frequencies
- Soft switching inverters (eg ZVS Class-D and Class-E) employ zero-voltage switching to minimise power dissipation
- Class-D inverters: popular with low-power systems adhering to Qi or A4WP standards
 - Lower normalised output power compared to Class-E
 - Require floating gate drive
 - But can operate over larger load range with ZVS if the switching frequency is below resonant frequency of output load network.



Class E

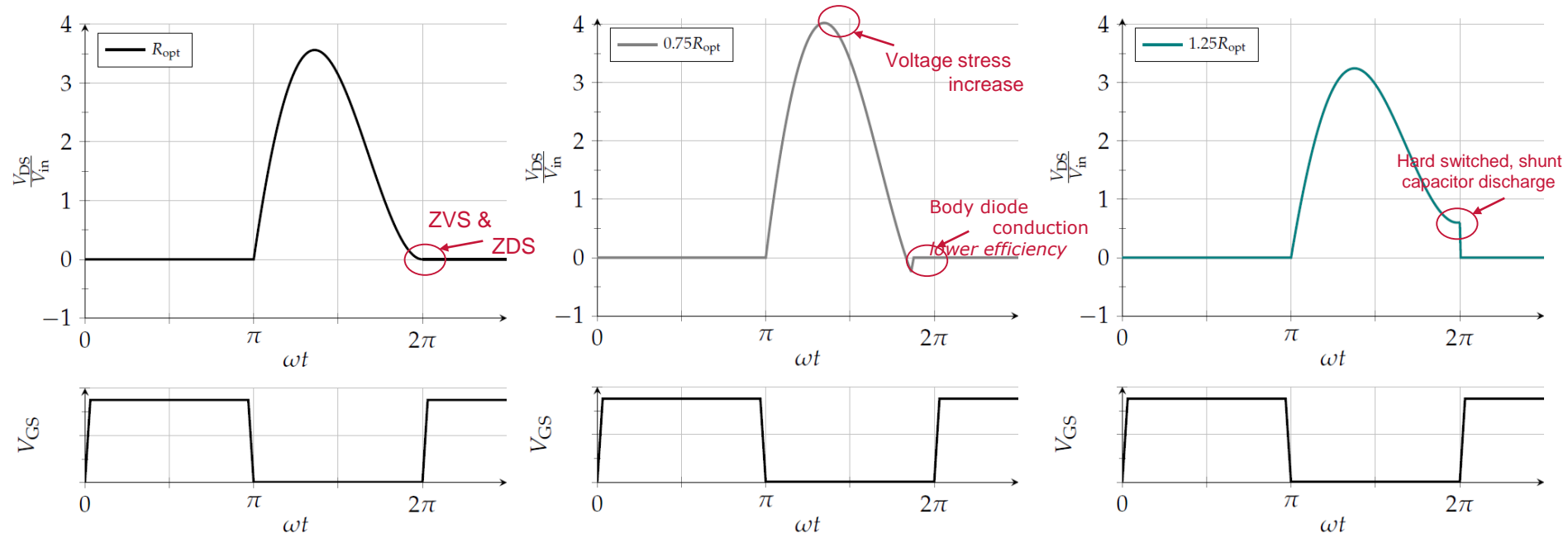
- Standard Class E circuit allows soft switching, and has only 1 switch, which is low side referenced. For this to be true, the load network is slightly inductive
- In this circuit, the load resistor is connected via an LC series circuit (operating slightly above the resonant frequency to present an inductive load) so that a square wave gate signal presents an almost pure sine wave voltage across the load



Graph from
https://www.eeweb.com/blog/alex_lidow/how-to-gan-gan-fets-for-high-frequency-wireless-power-transfer

Class E switching waveforms

Class E switching waveforms

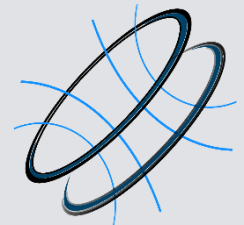


Optimum switching
 $R_L = R_{opt}$

Suboptimum switching
 $R_L < R_{opt}$

Non-optimum switching
 $R_L > R_{opt}$

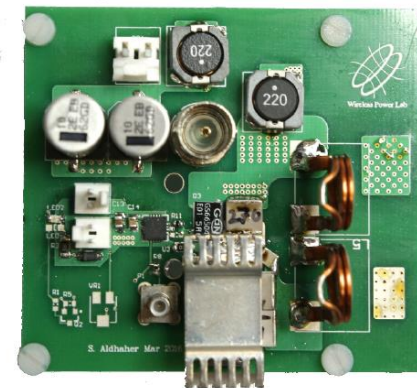
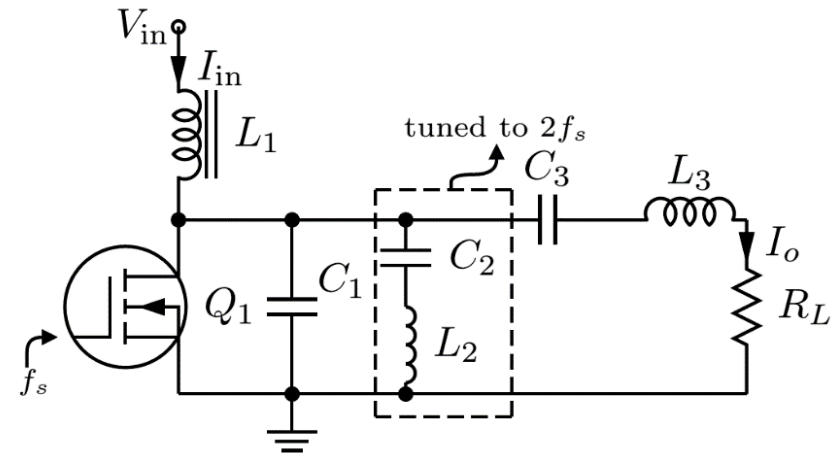
- Optimum switching operation is lost once the load shifts from its optimum value
- Voltages and current can be quite large



Load Independent Class EF Inverters

Class- EF_2 and Class- E/F_3 inverters

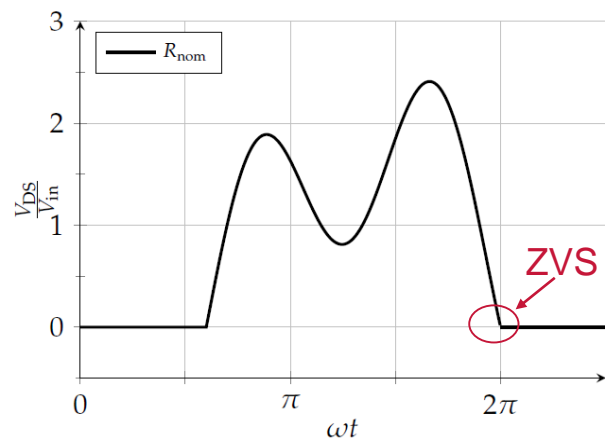
- Although Class-E inverters can achieve ZVS and ZCS, their voltage and current stresses can be large
- Adding series LC resonant network in parallel with MOSFET of Class-E inverter can reduce voltage and current stresses
 - Improved efficiency of inverter
 - Greater than twice the power handling
- Traditional to added network tuned to either 2nd harmonic (Class- EF_2) or 3rd harmonic (Class- E/F_3) of switching frequency
- However, tuning to around 1.5 times the resonant frequency allow load independent operation to be achieved



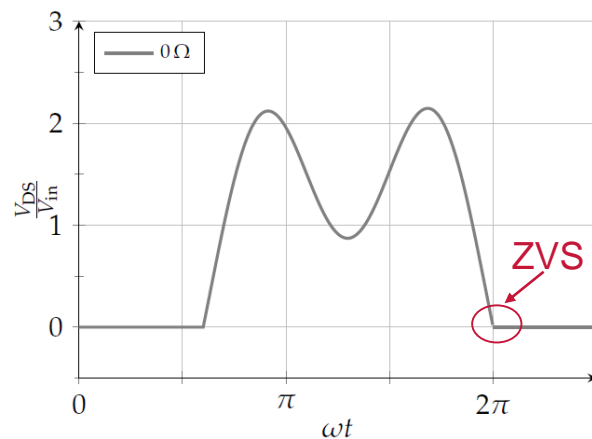


Load-independent Class EF inverter

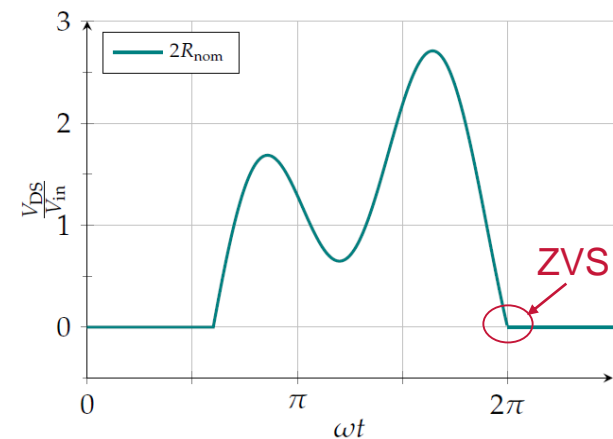
Tune the network to around 1.5 times the driving frequency



ZVS switching
 $R_L = R_{nom}$



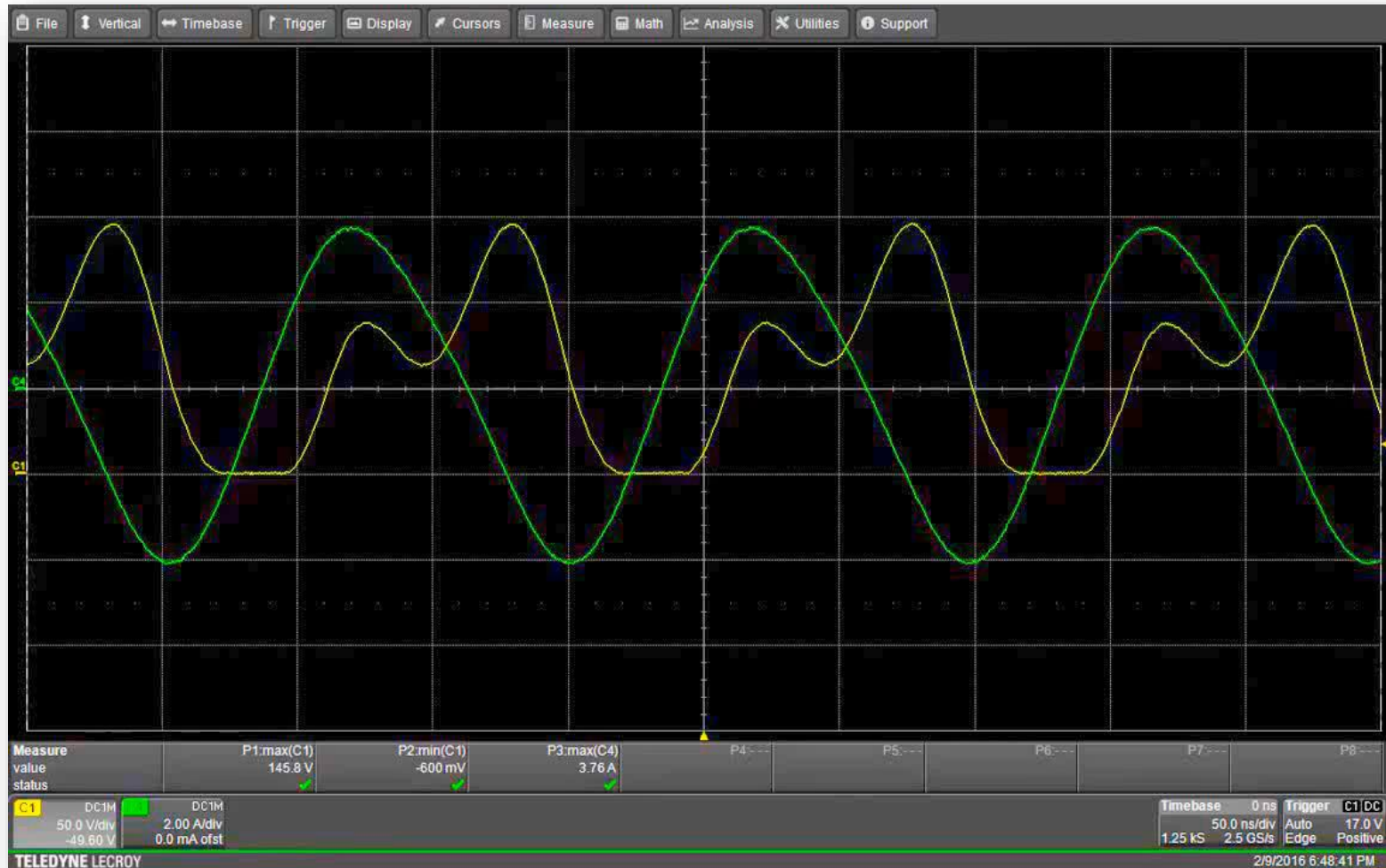
ZVS switching
 $R_L = 0$ (short circuit)



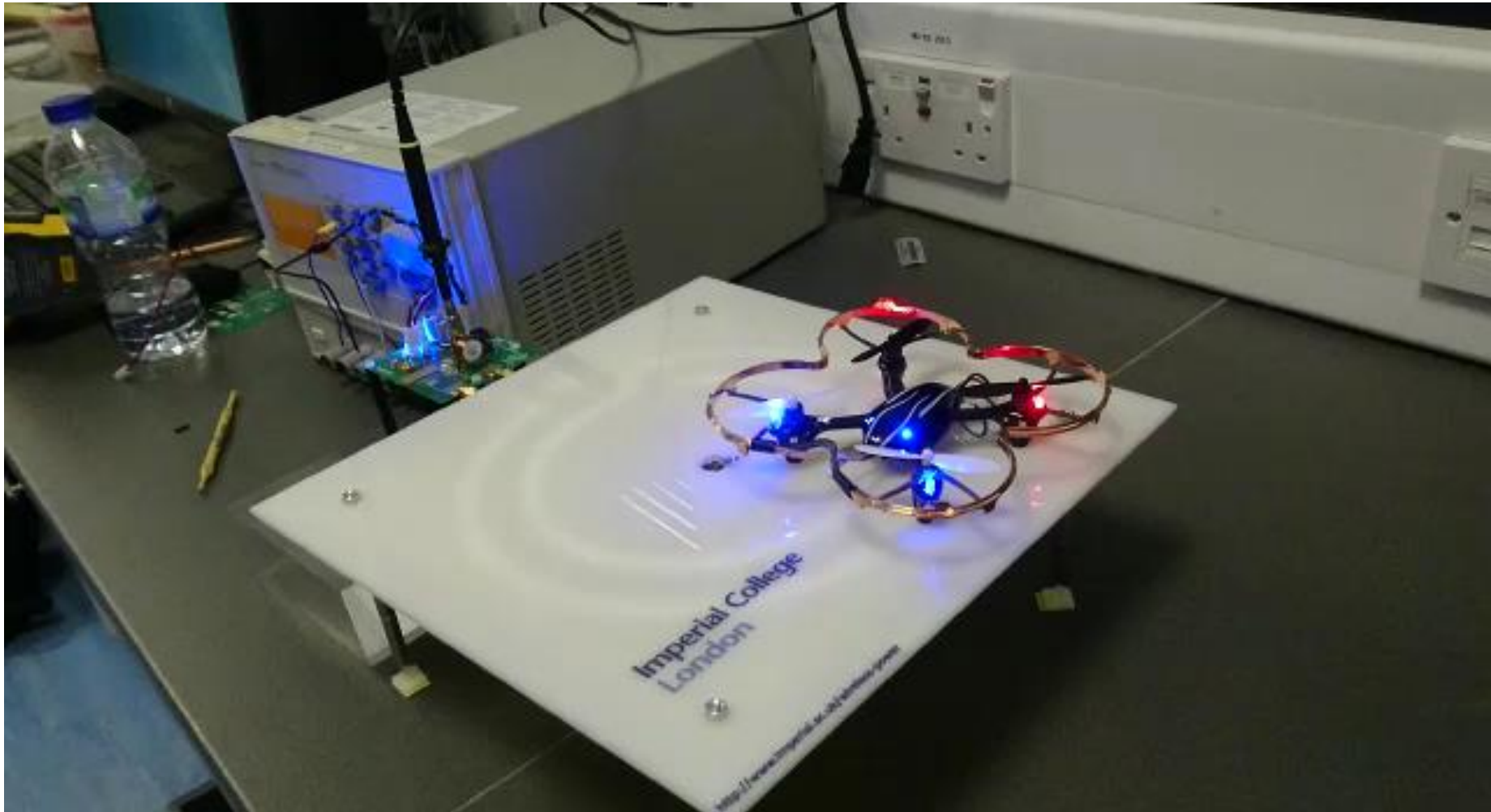
ZVS switching
 $R_L = 2R_{nom}$

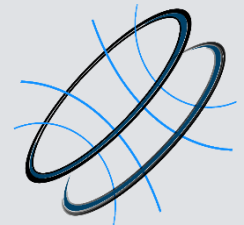
ZVS operation is maintained over a wide load range

Load-independent Operation with Constant Current



It Flies! Batteries NOT included!

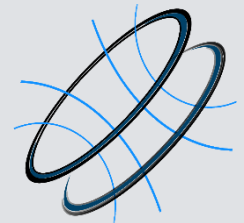




Conclusions

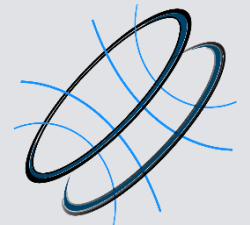
- Flying a drone via IPT is difficult because
 - Light weight
 - Rapidly varying load
 - Rapidly varying k
- Use series tuning to reflect a purely real load to the primary via use of a class D rectifier, or a class E with minimal input reactance change
- The load independent inverter can achieve zero voltage switching as k changes and as demand power changes
- The rectifier is constructed on a PCB around the size of a standard sim card
- The transmitter uses Gallium Nitride FETs to allow efficient operation

A century after Tesla – we can operate at much higher frequencies with high efficiency drive circuits and this gives us high Q , light-weight systems with low reliance on k



References

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- Link efficiency-led design of mid-range inductive power transfer systems, CH Kwan, G Kkelis, S Aldhafer, J Lawson, DC Yates, PCK Luk, Emerging Technologies: Wireless Power (WoW), 2015 IEEE PELS Workshop on, 1-7
- Maximizing DC-to-load efficiency for inductive power transfer, M Pinuela, DC Yates, S Lucyszyn, PD Mitcheson, Power Electronics, IEEE Transactions on 28 (5), 2437-2447



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- UK Government funding